## MILITARY HANDBOOK <br> RELIABILITY PREDICTION OF ELECTRONIC EQUIPMENT

To all holders of MIL-HDBK-217F

1. The following pages of MIL-HDBK-217F have been revised and supersede the pages isied.

| New Page(s) <br> vil | Date | Superseded Page(s) vii | Date <br> 2 Deoember 1991 |
| :---: | :---: | :---: | :---: |
| 5-3 |  | 5-3 | 2 December 1991 |
| 5-4 |  | 5-4 | 2 December 1991 |
| 5-7 |  | 5-7 | 2 December 1991 |
| 5-8 | 2 December 1991 | 5-8 | Reprinted without change |
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| 5-13 |  | 5-13 | 2 December 1991 |
| 5-14 | 2 December $19 \overline{9} 1$ | 5-14 | Reprinied without chañge |
| 5-19 |  | 5-19 | 2 December 1991 |
| 5-20 | 2 December 1991 | 5-20 | Reprinted without change |
| 6-15 |  | 6-15 | 2 December 1991 |
| 6-16 | 2 December 1991 | 6-16 | Feprinted without change |
| 7-1 | 2 December 1391 | $7=1$ | Peprinted without change |
| 7-2 |  | 7-2 | 2 December 1991 |
| 12-3 |  | 12-3 | 2 December 1991 |
| 12-4 | 2 December 1991 | 12-4 | Feprinted without change |
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| A-3 |  | A-3 | 2 December 1991 |
| A-4 | 2 December 1991 | A-4 | Reprinted without change |
| A-5 |  | A-5 | 2 Decemter 1391 |
| A-6 |  | A-6 | 2 December 1991 |
| A-7 |  | A-7 | 2 December 1991 |
| A-8 |  | A-8 | 2 December 1991 |
| A-9 |  | À-9 | 2 Decomter 1991 |
| A-10 | 2 December 1991 | A-10 | Reprinted without change |
| A-11 | 2 December 1991 | A-11 | Reprinted without change |
| A-12 |  | A-12 | 2 Decermber 1991 |
| A-13 |  | A-13 | 2 December 1991 |
| A-14 |  | A-14 | 2 December 1991 |
| A-15 | 2 December 1991 | A-15 | Reprinted without change |
| A-16 |  | A-16 | 2 December 1991 |

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## MIL-HDBK-217F NOTICE 1

2. Retain the pages of this notice and insert before the Table of Contents.
3. Holders of MIL-HDBK-217F will verify that page changes and additions indicated have been entered. The notice pages will be retained as a check sheet. The issuance, together with appended pages, is a separate priblication. Cach notice is to be retained by stocking points until the military handbook is revised or canceled.

Custodians:
Army - CR
Navy - EC
Air Force-17

Proparing Activity:
Air Force - 17.
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## Review Activities:

Anmy - MI, AV, ER
Navy - SH, AS, OS
Air Force - 11, 13, 14, 15, 18,
19, 99
User Activities:
Army - AT, ME, GL
Navy - CG, MC, YD, TD
Air Force - 85

## MIL-HDBK-217F NOTICE 1

MIL-HDBK-217F, Notice 1 is issued to correct minor typographical errors in the basic F Revision. MIL-HDBK-217F (base document) provides the following changes based upon recently completed studies (see Ref. 30 and 32 listed in Appendix C):

1. New failure rate prediction models are provided for the following nine major classes of microcircuits:

- Monolithic Bipolar Digital and Linear Gate/Logic Array Devices
- Monolithic MOS Digital and Linear Gate/Logic Array Devices
- Monolithic Bipolar and MOS Digital Microprocessor Devices (Including Controllers)
- Monolithic Bipolar and MOS Memory Devices
- Monolithic GaAs Digital Devices
- Monolithic GaAs MMIC Devices
- Hybrid Microcircuits
- Magnetic Bubble Memories
- Surface Acoustic Wave Devices

This revision provides new prediction models for bipolar and MOS microcircuits with gate counts up to 60,000, linear microcircuits with up to 3000 transistors, bipolar and MOS digital microprocessor and coprocessors up to 32 bits, memory devices with up to 1 million bits, GaAs monolithic microwave integrated circuits (MMICs) with up to 1,000 active elements, and GaAs digital ICs with up to 10,000 transistors. The $C_{\text {, }}$ factors have been extensively revised to reflect new technology devices with improved reliability, and the activation energies representing the temperature sensitivity of the dice ( $\pi_{T}$ ) have been changed for MOS devices and for memories. The $\mathrm{C}_{2}$ factor remains unchanged from the previous Handbook version, but includes pin grid arrays and surface mount packages using the same model as hermetic, solder-sealed dual in-line packages. New values have been included for the quality factor ( $\pi_{Q}$ ), the learning factor ( $\pi_{L}$ ), and the environmental factor ( $\pi_{E}$ ). The model for hybrid microcircuits has been revised to be simpler to use, to delete the temperature dependence of the seal and interconnect fallure rate contributions, and to provide a method of calculating chip junction temperatures.
2. A new model for Very High Speed Integrated Circuits (VHSICNHSIC Like) and Very Large Scale integration (VLSI) devices (gate counts above 60,000).
3. The reformatting of the entire handbook to make it easier to use.
4. A reduction in the number of environmental factors $\left(\pi_{E}\right)$ from 27 to 14.
5. A revised fallure rate model for Network Resistors.
6. Revised models for TWTs and Klystrons based on data supplied by the Electronic Industries Association Microwave Tube Division.

## DESCRIPTION

1. Bipolar Devices, Digital and Linear Gate/Logic Arrays
2. MOS Devices, Digital and Linear Gate/Logic Arrays
3. Field Programmable Logic Array (PLA) and

Programmable Array Logic (PAL)
4. Microprocessors

$$
\lambda_{P}=\left(C_{1} \pi_{T}+C_{2} \pi_{E}\right) \pi_{Q} \pi_{L} \text { Failures } / 10^{6} \text { Hours }
$$

Bipolar Digital and Linear Gate/Logic Array Die Complexity Faikure Rate - $\mathrm{C}_{1}$

| Digital |  | Linear |  |  | PLAPAL |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. Gates | $\mathrm{C}_{1}$ | No. Tran | sistors | $C_{1}$ | No. Gates | $\mathrm{C}_{1}$ |
| 1 to 100 | . 0025 | 1 to | 100 | . 010 | Up to 200 | . 010 |
| 101 to 1,000 | . 0050 | 101 to | 300 | . 020 | 201 to 1,000 | . 021 |
| 1,001 to 3,000 | . 010 | 30110 | 1,000 | . 040 | 1,001 to 5,000 | . 042 |
| 3,001 to 10,000 | . 020 | 1,001 to | 10,000 | . 060 |  |  |
| 10,001 to 30,000 | . 040 |  |  |  |  |  |
| 30,001 to 60,000 | . 080 |  |  |  |  |  |

MOS Digital and Linear Gate/Logic Array Die Complexity Failure Rate - C1 ${ }_{1}$

| Digital |  |  |  | Linear |  |  |  | PLAPAL |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. Gates |  |  | $C_{1}$ | No. | Tran | sistors | $C_{1}$ | No. Gates | $C_{1}$ |
| 1 | 10 | 100 | . 010 | 1 | 10 | 100 | . 010 | Up to 500 | . 00085 |
| 101 | to | 1,000 | . 020 | 101 | to | 300 | . 020 | 501 to 2,000 | . 0017 |
| 1.001 | to | 3,000 | . 040 | 301 | to | 1,000 | . 040 | 2,001 to 5,000 | . 0034 |
| 3,001 | to | 10,000 | . 080 | 1,001 |  | 10,000 | . 060 | 5,001 to 20,000 | . 0068 |
| 10,001 | to | 30,000 | . 16 |  |  |  |  |  |  |
| 30,001 | to | 60,000 | . 29 |  |  |  |  |  |  |

*NOTE: For CMOS gate counts above 60,000 use the VHSIC/VHSIC-Like model in Section 5.3

Microprocessor
Die Complexky Fallure Rate - $\mathrm{C}_{1}$

| No. Bits | Bipolar | MOS |
| :--- | :--- | :--- |
|  | $C_{1}$ | $C_{1}$ |
| Up to 16 | .060 | .14 |
| Up to 32 | .12 | .28 |

All Other Model Parameters

| Parameter | Refer to |
| :--- | :--- |
| $\pi_{\mathrm{T}}$ | Section 5.8 |
| $\mathrm{C}_{2}$ | Section 5.9 |
| $\pi_{\mathrm{E}}, \pi_{\mathrm{Q}}, \pi_{\mathrm{L}}$ | Section 5.10 |

## MIL-HDBK-217F <br> NOTICE 1

5.2 MICROCIRCUITS, MEMORIES

## DESCRIPTION

1. Read Only Memories (ROM)
2. Programmable Read Only Memories (PROM)
3. Utraviolet Eraseable PROMs (UVEPROM)
4. "Flash," MNOS and Floating Gate Electrically Eraseable PROMs (EEPROM). Includes both floating gate tunnel oxide (FLOTOX) and textured polysilicon type EEPROMs
5. Static Random Access Memories (SRAM)
6. Dynamic Random Access Memories (DRAM)

$$
\lambda_{D}=\left(C_{1} \pi_{T}+C_{2} \pi_{E}+\lambda_{c y c}\right) \pi_{Q} \pi_{L} \quad \text { Failures } / 10^{6} \text { Hours }
$$

Die Complexhy Fallure Rate $-\mathrm{C}_{1}$

| Memory Size, B (Bits) | MOS |  |  |  | Bipolar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROM | PROM, UVEPROM, EEPROM, EAPROM | DRAM | $\begin{gathered} \text { SRAM } \\ \text { (MOS \& } \\ \text { BiCMOS) } \end{gathered}$ | ROM, PROM | SRAM |
| Up to 16K | . 00065 | . 00085 | . 0013 | . 0078 | . 0094 | . 0052 |
| 16K < B $\leq 64 \mathrm{~K}$ | . 0013 | . 0017 | . 0025 | . 016 | . 019 | . 011 |
| $64 \mathrm{~K}<\mathrm{B} \leq 256 \mathrm{~K}$ | . 0026 | . 0034 | . 0050 | . 031 | . 038 | . 021 |
| $256 \mathrm{~K}<\mathrm{B} \leq 1 \mathrm{M}$ | . 0052 | . 0068 | . 010 | . 062 | . 075 | . 042 |


| A $_{1}$ Factor for $\lambda_{\text {cyc }}$ Calculation |  |  |
| :--- | :--- | :--- |
| Total No. of <br> Programming <br> Cycles Over <br> EEPROM Life, C  Flotox | Textured- <br> Poly $^{2}$ |  |
|  |  |  |
| Up to 100 | .00070 | .0097 |
| $100<C \leq 200$ | .0014 | .014 |
| $200<C \leq 500$ | .0034 | .023 |
| $500<C \leq 1 K$ | .0068 | .033 |
| $1 K<C \leq 3 K$ | .020 | .061 |
| $3 K<C \leq 7 K$ | .049 | .14 |
| $7 K<C \leq 15 K$ | .10 | .30 |
| $15 K<C \leq 20 K$ | .14 | .30 |
| $20 K<C \leq 30 K$ | .20 | .30 |
| $30 K<C \leq 100 K$ | .68 | .30 |
| $100 K<C \leq 200 K$ | 1.3 | .30 |
| $200 K<C \leq 400 K$ | 2.7 | .30 |
| $400 K<C \leq 500 K$ | 3.4 | .30 |

1. $A_{1}=6.817 \times 10^{-6}(C)$
2. No undertying equation for TexturedPoly.

| Total No. of Programming <br> Cycles Over EEPROM <br> Life, $C$ | Textured-Poly $A_{2}$ |
| :---: | :---: |
| Up to 300 K | 0 |
| $300 \mathrm{~K}<C \leq 400 \mathrm{~K}$ | 1.1 |
| $400 \mathrm{~K}<C \leq 500 \mathrm{~K}$ | 2.3 |

All Other Model Parameters

| Parameter | Refer to |
| :---: | :---: |
| $\pi_{T}$ | Section 5.8 |
| $C_{2}$ | Section 5.9 |
| $\pi_{E}, \pi_{Q}, \pi_{L}$ | Section 5.10 |
| $\lambda_{\text {cyc }}$ (EEPROMS only) | Page 5-5 |
| $\lambda_{\text {cyc }}=0 \quad$ For all other devices |  |

## DESCRIPTION

CMOS greater than 60:000 gates

$$
\lambda_{\mathrm{p}}=\lambda_{\mathrm{BD}} \pi_{M \mathrm{MFG}} \pi_{\mathrm{T}} \pi_{\mathrm{CD}}+\lambda_{\mathrm{BP}} \pi_{\mathrm{E}} \pi_{\mathrm{Q}} \pi_{\mathrm{PT}}+\lambda_{\mathrm{EOS}} \text { Failures/ } 10^{6} \text { Hours }
$$

Die Base Failure Rate $-\lambda_{\mathrm{BD}}$

| Pant Type | $\lambda_{\mathrm{BD}}$ |
| :--- | :--- |
| Logic and Custom | 0.16 |
| Gate Array and Memory | 0.24 |

Manufacturing Process Correction Factor - $\pi_{\text {MFG }}$

| Manufacturing Process | $\pi_{\text {MFG }}$ |
| :--- | :--- |
| QML or QPL | .55 |
| Non QML or Non QPL | 2.0 |

All Other Model Parameters

| Parameter | Refer to |
| :--- | :---: |
| $\pi_{\mathrm{T}}$ | Section 5.8 |
| $\pi_{\mathrm{E}}, \pi_{\mathrm{O}}$ | Section 5.10 |

Package Type Correction Factor $-\pi_{\text {PT }}$

|  | $\pi_{\text {PT }}$ |  |
| :--- | :---: | :---: |
| Package Type | Hermetic | Nonhermetic |
| DIP | 1.0 | 1.3 |
| Pin Grid Array | 2.2 | 2.9 |
| Chip Carrier | 4.7 | 6.1 |
| (Surface Mount |  |  |
| Technology) |  |  |

Die Complexity Correction Factor - $\pi_{C D}$

| Featurio Stzo (Microns) | A $\leq .4$ | . $4<A \leq .7$ | $\begin{gathered} \text { Die Area }\left(\mathrm{cm}^{2}\right) \\ .7<A \leq 1.0 \end{gathered}$ | $1.0<4 \leq 2.0$ | $2.0<A \leq 3.0$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| . 80 | 8.0 | 14 | 19 | 38 | 58 |
| 1.00 | 5.2 | 8.9 | 13 | 25 | 37 |
| 1.25 | 3.5 | 5.8 | 8.2 | 16 | 24 |
| ${ }^{\pi_{C D}}=\left(\left(\frac{A}{.24}\right)\left(\frac{2}{X_{s}}\right)^{2}(.64)\right)+.36 \quad A=$ Total Scribed Chip Die Area in $\mathrm{cm}^{2} \quad X_{s}=$ Feature Size (microns) <br> Die Area Conversion: $\mathrm{cm}^{2}=\mathrm{MIL}^{2} \div 155,000$ |  |  |  |  |  |

Package Base Failure Rate - $\lambda_{\mathrm{BP}}$

| Number oi Pins | $\lambda_{\mathrm{BP}}$ |
| :---: | ---: |
| 24 | .0026 |
| 28 | .0027 |
| 40 | .0029 |
| 44 | .0030 |
| 48 | .0030 |
| 52 | .0031 |
| 64 | .0033 |
| 84 | .0036 |
| 120 | .043 |
| 124 | .0043 |
| 144 | .0047 |
| 220 |  |
|  |  |
| $\lambda_{\mathrm{BP}}=.0022+\left(\left(1.72 \times 10^{-5}\right)(\mathrm{NP})\right)$ |  |
| $\mathrm{NP}=$ | Number of Package Pins |

Electrical Overstress Failure Rate - $\lambda_{E O S}$

| $V_{\text {TH }}$ (ESD Susceptibility (Voits)) ${ }^{\text {a }}$ | $\lambda_{\text {EOS }}$ |
| :---: | :---: |
| 0-1000 | . 065 |
| > 1000-2000 | . 053 |
| > 2000-4000 | . 044 |
| > 4000-16000 | . 029 |
| $>16000$ | . 0027 |
| $\lambda_{\text {EOS }}=\left(-\ln \left(1-.00057\right.\right.$ expl $\left.-.0002 V_{\text {TH }}\right)$ ) 100876 |  |
| $V_{T H}=$ ESD Susceptibility (volts) |  |
| - Voltage ranges which will cause the part to fail. If unknown, use $0-1000$ volts. |  |

## MIL-HDBK-217F

### 5.4 MICROCIRCUITS, GaAs MMIC AND DIGITAL DEVICES

## DESCRIPTION

Gallium Arsenide Microwave Monolithic Integrated Circuit (GaAs MMIC) and GaAs Digital Integrated Circuits using MESFET Transistors and Gold Based Metallization

$$
\lambda_{P}=\left[C_{1} \pi_{T} \pi_{A}+C_{2} \pi_{E}\right] \pi_{L} \pi_{Q} \text { Failures/106 Hours }
$$

| MMIC: Die Complexity Faikure Rates - $\mathrm{C}_{1}$ |
| :--- |
| Complexity <br> (No. of Elements) $\mathrm{C}_{1}$ <br> 1 to 100 4.5 <br> 101 to 1000 7.2 |

1. $\mathrm{C}_{1}$ accounts for the following active elements: transistors, diodes.

Digital: Die Complexity Failure Rates - $\mathrm{C}_{1}$

| Complexity <br> (No. of Elements) | $\mathrm{C}_{1}$ |
| :---: | :---: |
| 1 to 1000 | 25 |
| 1,001 to 10,000 | 51 |

1. $\mathrm{C}_{1}$ accounts for the following active elements: transistors, diodes.
Device Application Factor - $\pi_{\mathrm{A}}$

| Application | $\pi_{\mathrm{A}}$ |
| :--- | :---: |
| MMIC Devices |  |
| Low Noise \& Low Power ( $\leq 100 \mathrm{~mW}$ ) | 1.0 |
| Driver \& High Power (> 100 mW ) | 3.0 |
| Unknown | 3.0 |
| Digital Devices |  |
| All Digital Applications | 1.0 |

All Other Model Parameters

| Parameter | Refer to |
| :--- | :---: |
| $\pi_{T}$ | Section 5.8 |
| $C_{2}$ | Section 5.9 |
| $\pi_{E}, \pi_{L}, \pi_{\mathrm{O}}$ | Section 5.10 |

## DESCRIPTION

Hybrid Microcircuits

$$
\lambda_{P}=\left(\Sigma N_{C} \lambda_{C}\right)\left(1+.2 \pi_{E}\right) \pi_{F} \pi_{Q} \pi_{L} \text { Failures } / 10^{6} \text { Hours }
$$

$N_{c}=$ Number of Each Particular Component
$\lambda_{c}=$ Failure Rate of Each Particular Component

The general procedure for developing an overall hybrid failure rate is to calculate an individual failure rate for each component type used in the hybrid and then sum them. This summation is then modified to account for the overall hybrid function ( $\pi_{\mathrm{F}}$ ), screening level ( $\pi_{\mathrm{a}}$ ), and maturity ( $\pi_{\mathrm{L}}$ ). The hybrid package failure rate is a function of the active component failure modified by the environmental factor (i.e., ( $1+.2$ $\pi_{E}$ ) ). Onty the componert types tisted in the following table are considered to contribute significantly to
the overall failure rate of most hybrids. All other component types (e.g.. resistors, inductors, etc.) are considered to contribute insignificantly to the overall hybrid failure rate, and are assumed to have a failure rate of zero. This simplification is valid for most hybrids; however, if the hybrid consists of mostly passive components then a failure rate should be calculated for these devices. If factoring in other component types, assume $\pi_{Q}=1, \pi_{E}=1$ and $T_{A}=$ Hybrid Case Temperature for these calculations.

Determination of $\lambda_{c}$

| Determine $\lambda_{c}$ for These <br> Component Types | Handbook Section | Make These Assumptions When Determining <br> $\lambda_{C}$ |
| :--- | :---: | :--- |
| Microcircults | 5 | $C_{2}=0, \pi_{Q}=1, \pi_{L}=1, T_{J}$ as Determined from <br> Section $5.12, \lambda_{B P}=0$ (for VHSIC), <br> $\pi_{E}=1$ (for SAW). <br> Discrete Semiconductors <br> Capacitors$\quad 6$ |
| $\pi_{Q}=1, T_{J}$ as Determined from Section 6.14, <br> $\pi_{E}=1$. <br> $\pi_{Q}=1, T_{A}=$ Hybrid Case Temperature, <br> $\pi_{E}=1$. |  |  |

NOTE: If maximum rated stress for a die is unknown, assume the same as for a discretely package die of the same type. If the same die has several ratings based on the discrete packaged type, assume the lowest rating. Power rating used should be based on case temperature for discrete semiconductors.

Circult Function Factor - $\pi_{F}$

| Circuit Type | $\pi_{\mathrm{F}}$ |
| :--- | :---: |
|  |  |
| Digital | 1.0 |
| Video, $10 \mathrm{MHz}<\mathrm{f}<1 \mathrm{GHz}$ | 1.2 |
| Microwave, $\mathrm{f}>1 \mathrm{GHz}$ | 2.6 |
| Linear, $\mathrm{f}<10 \mathrm{MHz}$ | 5.8 |
| Power | 21 |

All Other Hybrid Model Parameters

| $\pi_{L}, \pi_{Q}, \pi_{E}$ | Refer to Section 5.10 |
| :---: | :--- |

## DESCRIPTION

Surface Acoustic Wave Devices

$$
\lambda_{P}=2.1 \pi_{Q} \pi_{E} \text { Failures } / 10^{6} \text { Hours }
$$

| Quality Factor $-\pi_{\mathrm{Q}}$ |
| :--- |
| Screening Levei $\pi_{\mathrm{Q}}$ <br> 10 Temperature Cycles $\left(-55^{\circ} \mathrm{C}\right.$ to <br> ＋125 <br> tests at temperature extremes． .10 <br> None beyond best commerical <br> practices． 1.0 |


| Environmental Factor $-\pi_{E}$ |  |
| :---: | :---: |
| Environment | $\pi_{E}$ |
| $\mathrm{G}_{\mathrm{B}}$ | .5 |
| $\mathrm{G}_{\mathrm{F}}$ | 2.0 |
| $\mathrm{G}_{\mathrm{M}}$ | 4.0 |
| $\mathrm{~N}_{\mathrm{S}}$ | 4.0 |
| $\mathrm{~N}_{\mathrm{U}}$ | 6.0 |
| $\mathrm{~A}_{\mathrm{K}}$ | 4.0 |
| $\mathrm{~A}_{\mathrm{IF}}$ | 5.0 |
| $\mathrm{~A}_{\mathrm{UC}}$ | 5.0 |
| $\mathrm{~A}_{\mathrm{UF}}$ | 8.0 |
| $\mathrm{~A}_{\mathrm{RW}}$ | 8.0 |
| $\mathrm{~S}_{\mathrm{F}}$ | .50 |
| $\mathrm{M}_{\mathrm{F}}$ | 5.0 |
| $\mathrm{M}_{\mathrm{L}}$ | 12 |
| $\mathrm{C}_{\mathrm{L}}$ | 220 |

## MIL-HDBK-217F

5.7 MICROCIRCUITS, MAGNETIC BUBBLE MEMORIES

The magnetic bubble memory device in its present form is a non-hermetic assembly consisting of the following two major structural segments:

1. A basic bubble chip or die consisting of memory or a storage area (e.g., an array of minor loops), and required control and detection elements (e.g., generators, various gates and detectors).
2. A magnetic structure to provide controlled magnetic fields consisting of permanent magnets, coils, and a housing.

These two structural segments of the device are interconnected by a mechanical substrate and lead frame. The interconnect substrate in the present technology is normally a printed circuit board. It should be noted that this model does not include external support microelectronic devices required for magnetic bubble memory operation. The model is based on Reference 33. The general form of the fallure rate model is:

$$
\lambda_{p}=\lambda_{1}+\lambda_{2} \text { Failures } / 10^{6} \text { Hours }
$$

where:
$\lambda_{1}=$ Failure Rate of the Control and Detection Structure
$\lambda_{1}=\pi_{Q}\left[N_{C} C_{11} \pi_{T_{1}} \pi_{W}+\left(N_{C} C_{21}+C_{2}\right) \pi_{E}\right] \pi_{D} \pi_{L}$
$\lambda_{2}=$ Failure Rate of the Memory Storage Area
$\lambda_{2}=\pi_{Q} N_{C}\left(C_{12} \pi_{T 2}+C_{22} \pi_{E}\right) \pi_{L}$

Chips Per Package - $\mathrm{N}_{\mathrm{C}}$
$N_{C}=$ Number of Bubble Chips per Packaged Device

Temperature Factor $-\pi_{T}$
$\pi_{T}=(.1) \exp \left[\frac{-E a}{8.63 \times 10^{-5}}\left(\frac{1}{T_{J}+273} \cdot \frac{1}{298}\right)\right]$
Use:
$E_{a}=.8$ to Calculate $\pi_{T 1}$
$\mathrm{E}_{\mathrm{a}}=.55$ to Calculate $\pi_{T 2}$
$T_{J}=$ Junction Temperature $\left({ }^{\circ} \mathrm{C}\right)$, $25 \leq T_{J} \leq 175$
$T_{J}=T_{\text {CASE }}+10^{\circ} \mathrm{C}$

Device Complexity Failure Rates for Control and Detection Structure - $\mathrm{C}_{11}$ and $\mathrm{C}_{21}$

$$
\begin{aligned}
C_{11}= & .00095\left(N_{1}\right) \cdot 40 \\
C_{21}= & .0004\left(N_{1}\right) \cdot 226 \\
N_{1}= & \begin{array}{l}
\text { Number of Dissipative Elements } \\
\text { on a Chip (gates, detectors, } \\
\text { generators, etc.), } N_{1} \leq 1000
\end{array}
\end{aligned}
$$

## MIL-HDBK-217F NOTICE 1

### 5.7 MICROCIRCUIT, MAGNETIC BUBBLE MEMORIES



Device Complexity Failure Rates for Memory Storage Structure $-\mathrm{C}_{12}$ and $\mathrm{C}_{22}$
$C_{12}=.00007\left(N_{2}\right)^{3}$
$C_{22}=.00001\left(N_{2}\right)^{.3}$
$N_{2}=$ Number of Bits, $N_{2} \leq 9 \times 10^{6}$

All Other Model Parameters

| Parameter | Section |
| :--- | :--- |
| $C_{2}$ | 5.9 |
| $\pi_{E}, \pi_{Q}, \pi_{L}$ | 5.10 |

Temperature Factor For All Microcircuits - $\pi$ r

|  | $\pm$ | 웅ㅇㅇㅇㅇ <br>  |
| :---: | :---: | :---: |
| $\begin{aligned} & \frac{0}{2} \\ & \frac{1}{2} \\ & \frac{0}{2} \end{aligned}$ | $\stackrel{\sim}{\square}$ | 8 8 8\% <br>  |
|  |  |  <br>  |
|  | 0 |  <br>  |
|  | $\stackrel{0}{0}$ |  |
| $\begin{aligned} & \underline{\underline{\mathbf{n}}} \\ & \underline{\underline{玉}} \end{aligned}$ | $\bigcirc$ |  <br>  |
|  |  |  <br>  |
|  | - |  |
|  |  |  |



### 5.9 MICROCIRCUITS, $C_{2}$ TABLE FOR ALL

Package Failure Rate for all Microcircuits - $\mathrm{C}_{2}$

| Package Type |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Number of Functional Pins, $N_{p}$ | Hermetic: DIPs w/Solder or Weld Seal, Pin Grid Array (PGA) ${ }^{1}$, SMT (Leaded and Nonleaded) | DIPs whth Glass Seal ${ }^{2}$ | Flatpacks with Axial Leads on 50 Mil Centers ${ }^{3}$ | Cans ${ }^{4}$ | Nonhermetic: DIPs, PGA. SMT (Leaded and Nonleaded) ${ }^{5}$ |
| 3 | . 00092 | . 00047 | . 00022 | . 00027 | 0012 |
| 4 | . 0013 | . 00073 | . 00037 | . 00049 | . 0016 |
| 6 | . 0019 | . 0013 | . 00078 | . 0011 | . 0025 |
| 8 | . 0026 | . 0021 | . 0013 | . 0020 | . 0034 |
| 10 | . 0034 | . 0029 | . 0020 | . 0031 | . 0043 |
| 12 | . 0041 | . 0038 | . 0028 | . 0044 | . 0053 |
| 14 | . 0048 | . 0048 | . 0037 | . 0060 | . 0062 |
| 16 | . 0056 | . 0059 | . 0047 | . 0079 | . 0072 |
| 18 | . 0064 | . 0071 | . 0058 |  | . 0082 |
| 22 | . 0079 | . 0096 | . 0083 |  | . 010 |
| 24 | . 0087 | . 011 | . 0098 |  | . 011 |
| 28 | . 010 | . 014 |  |  | . 013 |
| 36 | . 013 | . 020 |  |  | . 017 |
| 40 | . 015 | . 024 |  |  | . 019 |
| 64 | . 025 | . 048 |  |  | . 032 |
| 80 | . 032 |  |  |  | . 041 |
| 128 | . 053 |  |  |  | . 068 |
| 180 | . 076 |  |  |  | . 098 |
| 224 | . 097 |  |  |  | . 12 |

1. $C_{2}=2.8 \times 10^{-4}\left(N_{p}\right)^{1.08}$
2. $C_{2}=3.0 \times 10^{-5}\left(N_{p}\right)^{1.82}$
3. $C_{2}=3.6 \times 10^{-4}\left(N_{p}\right)^{1.08}$

## NOTES:

1. SMT: Surface Mount Technology
2. DIP: Dual In-Line Package
3. H DIP Sead type is unknown, assume gtass
4. The package fallure rate $\left(C_{2}\right)$ accounts for faikures associated only with the package inself.

Fallures assoclated with mounting the package to a circuit board are accounted for in Section 16, Interconnection Assemblies.

### 5.12 MICROCIRCUITS, $T_{J}$ DETERMINATION, (FOR HYBRIDS)

Typical Hybrid Characteristics

| Material | Typical Usage | Typical Thickness, $L_{i}$ (m.) | Feature From Figure 5-1 | $\begin{gathered} \text { Thermal } \\ \text { Conductivity, } \\ \mathrm{K}_{\mathrm{i}} \\ \left(\frac{\mathrm{~W} / \mathrm{in}^{2}}{{ }^{\circ} \mathrm{C} / \mathrm{in}}\right) \end{gathered}$ | $\begin{gathered} \left(\frac{1}{K_{i}}\right)\left(L_{i}\right) \\ \left(i^{2}{ }^{\circ} \mathrm{C} / \mathrm{w}\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Silicon | Chip Device | 0.010 | A | 2.20 | . 0045 |
| GaAs | Chip Device | 0.0070 | A | . 76 | . 0092 |
| Au Eutectic | Chip Attach | 0.0001 | B | 6.9 | . 000014 |
| Solder | Chip/Substrate Attach | 0.0030 | B/E | 1.3 | . 0023 |
| Epoxy (Dielectric) | Chip/Substrate Attach | 0.0035 | B/E | . 0060 | . 58 |
| Epoxy (Conductive) | Chip Attach | 0.0035 | B | . 15 | . 023 |
| Thick Fitm Dielectric | Glass Insulating Layer | 0.0030 | C | . 66 | . 0045 |
| Alumina | Substrate, MHP | 0.025 | D | . 64 | . 039 |
| Beryllium Oxide | Substrate, PHP | 0.025 | D | 6.6 | . 0038 |
| Kovar | Case, MHP | 0.020 | F | . 42 | . 048 |
| Aluminum | Case, MHP | 0.020 | F | 4.6 | . 0043 |
| Copper | Case, PHP | 0.020 | F | 9.9 | . 0020 |

NOTE: MHP: Multichip Hybrid Package, PHP: Power Hybrid Package (Pwr: $\geq 2 \mathrm{~W}$, Typically)

$$
\theta_{J C}=\frac{\sum_{i=1}^{n}\left(\frac{1}{K_{i}}\right)\left(L_{i}\right)}{A}
$$

$n=$ Number of Material Layers
$K_{i}=$ Thermal Conductivity of $i^{\text {th }}$ Material $\left(\frac{W / i^{2}}{{ }^{2} / / \mathrm{n}}\right)$ (User Provided or From Table)
$L_{1} \quad$ - Thickness of ith Material (in) (User Provided or From Table)
A = Die Area (in ${ }^{2}$ ). If Die Area cannot be readily determined, estimate as fotlows: $A=[.00278 \text { (No. of Die Active Wire Terminals) }+.0417]^{2}$

Estimate $T_{J}$ as Follows:

$$
T_{J}=T_{C}+\left(\theta_{J C}\right)\left(P_{D}\right)
$$

$T_{C}=$ Hybrid Case Temperature $\left({ }^{\circ} \mathrm{C}\right)$. H unknown, use the $T_{C}$ Default Table shown in Section 5.11.
$\theta_{\mathrm{JC}}=$ Junction-to-Case Thermal Resistance ( ${ }^{\circ} \mathrm{CM}$ ) (As determined above)
$P_{D}=$ Die Power Dissipation (W)

## Example 1: CMOS Digital Gate Array

Given: A CMOS digital timing chip (4046) in an airbome inhabited cargo application, case temperature $48^{\circ} \mathrm{C}, 75 \mathrm{~mW}$ power dissipation. The device is procured with normal manufacturer's screening consisting of temperature cycling, constant acceleration, electrical testing, seal test and extemal visual inspection, in the sequence given. The component manufacturer atso performs a B-level burn-in followed by electrical testing. All screens and tests are performed to the applicable MIL-STD-883 screening method. The package is a 24 pin ceramic DIP with a glass seal. The device has been manufactured for several years and has 1000 transistors.

$$
\lambda_{P}=\left(C_{1} \pi_{T}+C_{2} \pi_{E}\right) \pi_{Q} \pi_{L} \quad \text { Section } 5.1
$$



## Example 2: EEPROM

Given: A 128 K Fiotox EEPROM that is expected to have a $T_{J}$ of $80^{\circ} \mathrm{C}$ and experience 10,000 read/write cycles over the life of the system. The part is procured to all requirements of Paragraph 1.2.1, MIL-STD-883, Class B screening level requirements and has been in production for three years. His packaged in a 28 pin DIP with a glass seal and will be used in an airborne uninhabited cargo application.

$$
\pi_{P}=\left(C_{1} \pi_{T}+C_{2} \pi_{E}+\lambda_{\text {cyc }}\right) \pi_{Q} \pi_{L} \quad \text { Section } 5.2
$$

| $C_{1}=.0034$ | Section 5.2 |
| :--- | :--- | :--- |
| $\pi_{T}=3.8$ | Section 5.8 |
| $C_{2}=.014$ | Section 5.9 |

## MIL-HDBK-217F NOTICE 1

### 6.8 TRANSISTORS, HIGH FREQUENCY, GaAs FET

Matching Network Factor $-\pi_{M}$

| Matching | $\pi_{M}$ |
| :--- | :---: |
| Input and Output | 1.0 |
| Input Only | 2.0 |
| None | 4.0 |


| Environment Factor $-\pi_{E}$ |  |
| :---: | :---: |
| Environment | $\pi_{E}$ |
| $G_{B}$ | 1.0 |
| $G_{F}$ | 2.0 |
| $G_{M}$ | 5.0 |
| $N_{S}$ | 4.0 |
| $N_{U}$ | 11 |
| $A_{K_{C}}$ | 4.0 |
| $A_{I F}$ | 5.0 |
| $A_{U C}$ | 7.0 |
| $A_{U F}$ | 12 |
| $A_{R W}$ | 16 |
| $S_{F}$ | .50 |
| $M_{F}$ | 9.0 |
| $M_{L}$ | 24 |
| $C_{L}$ | 250 |

## MIL-HDBK-217F

6.9 TRANSISTORS, HIGH FREQUENCY, SI FET

## SPECIFICATION

MIL-S-19500

## DESCRIPTION

Si FETs (Avg. Power < 300 mW . Freq. > 400 MHz )

$$
\lambda_{p}=\lambda_{b} \pi_{T} \pi_{Q} \pi_{E} \quad \text { Failures } / 10^{6} \text { Hours }
$$

| Base Faikure Rate $-\lambda_{\mathrm{b}}$ |  |
| :--- | :---: |
| Transistor Type $\lambda_{\mathrm{b}}$ <br> MOSFET .060 <br> JFET .023 |  |


| $\mathrm{T}_{\mathrm{J}}\left({ }^{\circ} \mathrm{C}\right)$ | ${ }_{T}$ | $\left.\mathrm{T}_{3}{ }^{\circ} \mathrm{C}\right)$ | $\pi_{T}$ |
| :---: | :---: | :---: | :---: |
| 25 | 1.0 | 105 | 3.9 |
| 30 | 1.1 | 110 | 4.2 |
| 35 | 1.2 | 115 | 4.5 |
| 40 | 1.4 | 120 | 4.8 |
| 45 | 1.5 | 125 | 5.1 |
| 50 | 1.6 | 130 | 5.4 |
| 55 | 1.8 | 135 | 5.7 |
| 60 | 2.0 | 140 | 6.0 |
| 65 | 2.1 | 145 | 6.4 |
| 70 | 2.3 | 150 | 6.7 |
| 75 | 2.5 | 155 | 7.1 |
| 80 | 2.7 | 160 | 7.5 |
| 85 | 3.0 | 165 | 7.9 |
| 90 | 3.2 | 170 | 8.3 |
| 95 | 3.4 | 175 | 8.7 |
| 100 | 3.7 |  |  |
| $\pi_{T}=\exp \left(-1925\left(\frac{1}{T_{J}+273} \cdot \frac{1}{298}\right)\right)$ |  |  |  |
| $T_{J}=$ Junction Tomperature ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |


| Quality Factor - $\pi_{\mathrm{Q}}$ |  |
| :--- | :---: |
| Quality | $\pi_{\mathrm{Q}}$ |
| JANTXV | .50 |
| JANTX | 1.0 |
| JAN | 2.0 |
| Lower | 5.0 |


| Environment Factor $-\pi_{E}$ |  |
| :---: | :---: |
| Environment | $\pi_{E}$ |
| $G_{B}$ | 1.0 |
| $G_{F}$ | 2.0 |
| $G_{M}$ | 5.0 |
| $N_{S}$ | 4.0 |
| $N_{U}$ | 11 |
| $A_{I C}$ | 4.0 |
| $A_{I F}$ | 5.0 |
| $A_{U C}$ | 7.0 |
| $A_{U F}$ | 12 |
| $A_{R W}$ | 16 |
| $s_{F}$ | .50 |
| $M_{F}$ | 24.0 |
| $M_{L}$ | 250 |

## DESCRIPTION

All Types Except Traveling Wave Tubes and Magnetrons. Includes Receivers, CRT, Thyratron, Crossed Field Amplifier, Pulsed Gridded, Transmitting, Vidicons, Twystron, Pulsed Klystron, CW Klystron

$$
\lambda_{p}=\lambda_{b} \pi_{L} \pi_{E} \text { Failures } / 10^{6} \text { Hours }
$$

Base Failure Rate - $\lambda_{b}$


### 7.1 TUBES, ALL TYPES EXCEPT TWT AND MAGNETRON

Alternate* Base Failure Rate for Putsed Klystrons - $\lambda_{6}$

| P(MW | .2 | .4 | .6 | .8 | 1.0 | 2.0 | 4.0 | 6.0 |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| .01 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 |
| .30 | 16 | 16 | 17 | 17 | 17 | 18 | 20 | 21 |
| .80 | 16 | 17 | 17 | 18 | 18 | 21 | 25 | 30 |
| 1.0 | 17 | 17 | 18 | 18 | 19 | 22 | 28 | 34 |
| 3.0 | 18 | 20 | 21 | 23 | 25 | 34 | 51 |  |
| 5.0 | 19 | 22 | 25 | 28 | 31 | 45 | 75 |  |
| 8.0 | 21 | 25 | 30 | 35 | 40 | 63 | 110 |  |
| 10 | 22 | 28 | 34 | 40 | 45 | 75 |  |  |
| 25 | 31 | 45 | 60 | 75 | 90 | 160 |  |  |

$\lambda_{B}=2.94(F)(P)+16$
$F=$ Operating Frequency in $\mathrm{GHz}, 0.2 \leq F \leq 6$
$P=P e a k$ Output Power in MW, . $01 \leq P \leq 25$ and $P \leq 490 F^{-2.95}$
-See previous page for other Klystron Base Failure Rates.

Alternate* Base Failure Rate for CW Klystrons - $\lambda_{b}$

| P(KW) | 300 | 500 | 800 | 1000 | $F(M H z)$ | 2000 | 4000 | 6000 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 0.1 | 30 | 31 | 33 | 34 | 38 | 47 | 57 | 66 |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.0 | 31 | 32 | 33 | 34 | 39 | 48 | 57 | 66 |
| 3.0 | 32 | 33 | 34 | 35 | 40 | 49 | 58 |  |
| 5.0 | 33 | 34 | 35 | 36 | 41 | 50 |  |  |
| 8.0 | 34 | 35 | 37 | 38 | 42 |  |  |  |
| 10 | 35 | 36 | 38 | 39 | 43 |  |  |  |
| 30 | 45 | 46 | 48 | 49 |  |  |  |  |
| 50 | 55 | 56 | 58 | 59 |  |  |  |  |
| 80 | 70 | 71 | 73 |  |  |  |  |  |
| 100 | 80 | 81 |  |  |  |  |  |  |

$\lambda_{b}=0.5 P+.0046 F+29$
$P=$ Average Output Power in KW, $0.1 \leq P \leq 100$ and $P \leq 8.0(10)^{6}(F)^{-1.7}$
$F=$ Operating Frequency in MHz . $300 \leq F \leq 8000$

## -See previous page for other Klystron Base Failure Rates.

| Leaming Factor $-\pi_{L}$ |  |
| :---: | :---: |
| $T$ (years) | $\pi_{L}$ |
| $\leq 1$ | 10 |
| 2 | 2.3 |
| $\geq 3$ | 1.0 |
| $\pi_{L}$ | $=10(T)^{-2.1}, 1 \leq T \leq 3$ |
|  | $=10, T \leq 1$ |
| $T$ | $=1 . T \geq 3$ |$\quad$| Number of Years since Introduction |
| :--- |
| to Field Use |

Environment Factor $-\pi_{E}$

| Environment | $\pi_{E}$ |
| :---: | :---: |
| $\mathrm{G}_{8}$ | . 50 |
| $\mathrm{G}_{\mathrm{F}}$ | 1.0 |
| $\mathrm{G}_{\mathrm{M}}$ | 14 |
| $\mathrm{N}_{\mathrm{S}}$ | 8.0 |
| $\mathrm{N}_{\mathrm{U}}$ | 24 |
| $A_{1 C}$ | 5.0 |
| $A_{\text {IF }}$ | 8.0 |
| ${ }^{\text {A }}$ UC | 6.0 |
| $A_{\text {UF }}$ | 12 |
| $A_{\text {RW }}$ | 40 |
| $S_{F}$ | . 20 |
| $M_{F}$ | 22 |
| $M_{L}$ | 57 |
| $C_{L}$ | 1000 |

## MIL-HDBK-217F NOTICE 1

### 12.2 ROTATING DEVICES, SYNCHROS AND RESOLVERS

## DESCRIPTION

Rotating Synchros and Resolvers

$$
\lambda_{p}=\lambda_{b} \pi_{S} \pi_{N} \pi_{E} \text { Failures/10 Hours }
$$

NOTE: Synchros and resolvers are predominately used in service requiring only slow and infrequent motion. Mechanical wearout problems are infrequent so that the electrical failure mode dominates, and no mechanical mode failure rate is required in the model above.


## MIL-HDBK-217F

### 12.3 ROTATING DEVICES, ELAPSED TIME METERS

DESCRIPTION Elapsed Time Meters

$$
\lambda_{p}=\lambda_{b} \pi_{T} \pi_{E} \text { Failures } / 10^{6} \text { Hours }
$$

| Base Failure Rate $-\lambda_{b}$ |  |
| :--- | :---: |
| Type $\lambda_{\mathrm{b}}$ <br> A.C. 20 <br> Inverter Driven 30 <br> Commutator D.C. 80 |  |

Environment Factor $-\pi_{E}$

| Environment | $\pi_{E}$ |
| :---: | :---: |
| $G_{B}$ | 1.0 |
| $G_{F}$ | 2.0 |
| $G_{M}$ | 12 |
| $N_{S}$ | 7.0 |
| $N_{U}$ | 18 |
| $A_{K}$ | 5.0 |
| $A_{I F}$ | 8.0 |
| $A_{U C}$ | 16 |
| $A_{U F}$ | 25 |
| $A_{R W}$ | 26 |
| $S_{F}$ | .50 |
| $M_{F}$ | 14 |
| $M_{L}$ | 38 |
| $C_{L}$ | $N / A$ |

## APPENDIX A: PARTS COUNT RELIABILITY PREDICTION

Parts Count Rellabllity Prediction - This prediction method is applicable during bid proposal and earty design phases when insufficient information is available to use the part stress analysis models shown in the main body of this Handbook. The information needed to apply the method is (1) generic pant types (including complexity for microcircuits) and quantities, (2) part quality levels, and (3) equipment environment. The equipment taiture rate is obtained by looking up a generic failure rate in one of the following tables, multiplying it by a quality factor, and then summing it with failure rates obtained for other components in the equipment. The general mathematical expression for equipment failure rate with this method is:

$$
\lambda_{\text {EQUIP }}=\sum_{i=1}^{i=n} N_{i}\left(\lambda_{g} \pi_{0}\right)_{i} \quad \text { Equation } 1
$$

for a given equipment environment where:

| $\lambda_{\text {EQUIP }}$ | $=$ Total equipment fallure rate (Failures/ $10^{6}$ Hours) |
| :--- | :--- |
| $\lambda_{g}$ | $=$ Generic failure rate for the $i^{\text {th }}$ generic part (Failures $/ 10^{6}$ Hours) |
| $\pi_{Q}$ | $=$ Quality factor for the $i^{\text {th }}$ generic part |
| $N_{i}$ | $=$ Quantity of $i^{\text {th }}$ generic part |
| $n$ | $=$ Number of different generic part categories in the equipment |

Equation 1 applies if the entire equipment is being used in one environment. If the equipment comprises several units operating in different environments (such as avionics systems with units in airborne inhabited $\left(A_{1}\right)$ and uninhabited ( $A_{U}$ ) environments), then Equation 1 should be applied to the portions of the equipment in each environment. These "environment-equipment" failure rates should be added to determine total equipment failure rate. Environmental symbols are defined in Section 3.

The quality factors to be used with each part type are shown with the applicable $\lambda_{\mathrm{g}}$ tables and are not necessarily the same values that are used in the Part Stress Analysis. Microcircuits have an additional multiplying factor, $\pi_{\mathrm{L}}$, which accounts for the maturity of the manufacturing process. For devices in production two years or more, no moditication is needed. For those in production less than two years, $\lambda_{g}$ should be multiplied by the appropriate in factor (See page A-4).

It should be noted that no generic falure rates are shown for hybrid microchrcults. Each hybrid is a faily unique device. Since none of these devices have been standardized, their complexity cannot be determined from their name or function. Ldentically or similarly named hybrids can have a wide range of complexity that thwarts categorization for purposes of this prediction method. If hybrids are anticipated for a design, their use and construction should be thoroughly investigated on an individual basis with application of the prediction model in Section 5.

The fallure rates shown in this Appendix were calculated by assigning model default values to the failure rate models of Section 5 through 23. The specitic defaul values used for the model parameters are shown with the $\lambda_{\mathrm{g}}$ Tables for microcircuits. Defaull parameters for all other pan classes are summarized in the tables starting on Page A-12. For parts with characteristics which differ significantly from the assumed defaults, or parts used in large quantities, the underlying models in the main body of this Handbook can be used.

## MIL-HDBK-217F NOTICE 1

APPENDIX A: PARTS COUNT

| $\begin{gathered} \text { Section } \\ \\ \hline \end{gathered}$ | Paritype | $\begin{aligned} & \text { Enmion. } \rightarrow \\ & T_{J}(C) \rightarrow \\ & \hline \end{aligned}$ | $\begin{aligned} & G_{8} \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & G_{F} \\ & 60 \\ & \hline \end{aligned}$ | $\begin{aligned} & G_{M} \\ & 65 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{N}_{\mathrm{S}} \\ & 60 \\ & \hline \end{aligned}$ | $\begin{aligned} & N_{u} \\ & 65 \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{1 C} \\ & 75 \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{\text {IF }} \\ & 75 \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{A}_{\text {UC }} \\ 90 \\ \hline \end{gathered}$ | $\begin{aligned} & A_{1 F} \\ & 90 \\ & \hline \end{aligned}$ | $\begin{gathered} A_{\text {RW }} \\ 75 \\ \hline \end{gathered}$ | $\begin{aligned} & S_{F} \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { TF } \\ & 85 \\ & \hline \end{aligned}$ | $\begin{aligned} & M_{L} \\ & 75 \\ & \hline \end{aligned}$ | $\begin{aligned} & C_{L} \\ & -60 \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.1 |  |  | $\begin{aligned} & .0036 \\ & .0060 \\ & .011 \\ & .033 \\ & .052 \\ & .075 \end{aligned}$ | $\begin{aligned} & .012 \\ & .020 \\ & .035 \\ & .12 \\ & .17 \\ & .23 \\ & \hline \end{aligned}$ | $\begin{aligned} & .024 \\ & .038 \\ & .066 \\ & .22 \\ & .33 \\ & .44 \\ & \hline \end{aligned}$ | $\begin{aligned} & .024 \\ & .037 \\ & .085 \\ & .22 \\ & .33 \\ & .43 \\ & \hline \end{aligned}$ | $\begin{aligned} & .035 \\ & .055 \\ & .097 \\ & .33 \\ & .48 \\ & .83 \\ & \hline \end{aligned}$ | $\begin{aligned} & .025 \\ & .039 \\ & .070 \\ & .23 \\ & .34 \\ & .46 \\ & \hline \end{aligned}$ | $\begin{aligned} & .030 \\ & .48 \\ & .085 \\ & .28 \\ & .42 \\ & .58 \\ & \hline \end{aligned}$ | $\begin{aligned} & .032 \\ & .051 \\ & .091 \\ & .30 \\ & .45 \\ & .81 \\ & \hline \end{aligned}$ | .049 <br> .077 <br> .14 <br> .46 <br> .68 <br> .90 | $\begin{aligned} & .047 \\ & .074 \\ & .13 \\ & .44 \\ & .65 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0038 \\ & .0060 \\ & .011 \\ & .033 \\ & .052 \\ & .075 \\ & \hline \end{aligned}$ | .030 .048 .082 .28 .41 .53 | $\begin{gathered} .069 \\ .11 \\ .19 \\ .65 \\ .95 \\ 1.2 \\ \hline \end{gathered}$ | $\begin{array}{r} 1.2 \\ 1.9 \\ 3.3 \\ 12 \\ 17 \\ 21 \\ \hline \end{array}$ |
| 5.1 |  <br> 1-100 Trercivivir <br> 101 - 320 Tranadetors <br> 301 - 4000 Tremiliotions <br> 1001 - 10.000 Tranderars | ( 14 Pn DPP) (18 Pin DP') (24 Pin DP ( 40 Pin DP | $\begin{aligned} & .0095 \\ & .017 \\ & .003 \\ & .050 \\ & \hline \end{aligned}$ | $\begin{aligned} & .024 \\ & .041 \\ & .074 \\ & .12 \\ & \hline \end{aligned}$ | $\begin{aligned} & .039 \\ & .085 \\ & .11 \\ & .18 \\ & \hline \end{aligned}$ | $\begin{aligned} & .051 \\ & .051 \\ & .092 \\ & .15 \\ & \hline \end{aligned}$ | $\begin{array}{r} .049 \\ .078 \\ .13 \\ .21 \\ \hline \end{array}$ | $\begin{array}{r} .057 \\ .10 \\ .19 \\ .29 \\ \hline \end{array}$ | $\begin{aligned} & .062 \\ & .11 \\ & .19 \\ & .30 \\ & \hline \end{aligned}$ | $\begin{array}{r} .12 \\ .22 \\ .41 \\ .63 \\ \hline \end{array}$ | $\begin{array}{r} .13 \\ .24 \\ .44 \\ .67 \\ \hline \end{array}$ | $\begin{aligned} & .076 \\ & .13 \\ & .32 \\ & .35 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0095 \\ & .017 \\ & .033 \\ & .050 \\ & \hline \end{aligned}$ | $\begin{aligned} & .044 \\ & .072 \\ & .12 \\ & .18 \\ & \hline \end{aligned}$ | .098 <br> .15 <br> .28 <br> .41 | $\begin{aligned} & 1.1 \\ & 1.4 \\ & 2.0 \\ & 3.4 \\ & \hline \end{aligned}$ |
| 5.1 |  |  | $\begin{aligned} & .0061 \\ & .011 \\ & .022 \\ & \hline \end{aligned}$ | $\begin{array}{r} .010 \\ .020 \\ .055 \end{array}$ | $\begin{aligned} & .029 \\ & .048 \\ & .087 \end{aligned}$ | $\begin{aligned} & .027 \\ & .0415 \\ & .002 \\ & \hline \end{aligned}$ | $\begin{aligned} & .040 \\ & .065 \\ & .12 \\ & \hline \end{aligned}$ | $\begin{array}{r} .032 \\ .054 \\ .099 \\ \hline \end{array}$ | $\begin{array}{r} .037 \\ .063 \\ .11 \\ \hline \end{array}$ | $\begin{aligned} & .044 \\ & .077 \\ & .14 \\ & \hline \end{aligned}$ | $\begin{aligned} & .061 \\ & .10 \\ & .19 \\ & \hline \end{aligned}$ | $\begin{array}{r} .054 \\ .089 \\ .16 \\ \hline \end{array}$ | $\begin{array}{r} .0081 \\ .011 \\ .022 \\ \hline \end{array}$ | $\begin{array}{r} .034 \\ .057 \\ .10 \\ \hline \end{array}$ | $\begin{aligned} & .076 \\ & .12 \\ & .22 \\ & \hline \end{aligned}$ | 1.2 <br> 1.9 <br> 3.3 |
| 5.1 |  | (16 PM DPP) ( 24 Pm DP ${ }^{2}$ ) ( 40 Pm DPP) (12: Pin PaA) ( 180 Pm PGA) (224 Pin PGA) | .0057 .010 .019 .048 .084 .13 | $\begin{aligned} & .015 \\ & .028 \\ & .047 \\ & .14 \\ & .22 \\ & .31 \\ & \hline \end{aligned}$ | $\begin{aligned} & .027 \\ & .045 \\ & .080 \\ & .25 \\ & .38 \\ & .53 \\ & \hline \end{aligned}$ | $\begin{aligned} & .027 \\ & .043 \\ & .077 \\ & .24 \\ & .37 \\ & .51 \\ & \hline \end{aligned}$ | $\begin{aligned} & .039 \\ & .082 \\ & .11 \\ & .38 \\ & .54 \\ & .73 \\ & \hline \end{aligned}$ | $\begin{aligned} & .029 \\ & .049 \\ & .088 \\ & .27 \\ & .42 \\ & .59 \\ & \hline \end{aligned}$ | $\begin{aligned} & .035 \\ & .057 \\ & .10 \\ & .32 \\ & .49 \\ & .69 \\ & \hline \end{aligned}$ | $\begin{aligned} & .030 \\ & .018 \\ & .18 \\ & .38 \\ & .82 \\ & .82 \\ & \hline \end{aligned}$ | .056 <br> .092 <br> .17 <br> .71 <br> .79 | $\begin{aligned} & .052 \\ & .033 \\ & .15 \\ & .48 \\ & .72 \\ & .98 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0057 \\ & .010 \\ & .019 \\ & .049 \\ & .084 \\ & .13 \\ & \hline \end{aligned}$ | $\begin{aligned} & .033 \\ & .053 \\ & .095 \\ & .30 \\ & .46 \\ & .63 \\ & \hline \end{aligned}$ | $\begin{array}{r} .074 \\ .12 \\ .21 \\ .89 \\ 1.0 \\ 1.4 \\ \hline \end{array}$ | $\begin{array}{r} 1.2 \\ 1.9 \\ 3.3 \\ 12 \\ 17 \\ 21 \\ \hline \end{array}$ |
| 5.1 | $\qquad$ |  | .0095 <br> .017 <br> .033 | $\begin{array}{r} .024 \\ .041 \\ .074 \\ .12 \\ \hline \end{array}$ | $\begin{aligned} & .039 \\ & .065 \\ & .11 \\ & .18 \\ & \hline \end{aligned}$ | $\begin{aligned} & .034 \\ & .054 \\ & .092 \\ & .15 \\ & \hline \end{aligned}$ | .049 <br> .078 <br> .13 <br> .21 | $\begin{aligned} & .057 \\ & .10 \\ & .19 \\ & .29 \\ & \hline \end{aligned}$ | $\begin{aligned} & .062 \\ & .11 \\ & .19 \\ & .30 \\ & \hline \end{aligned}$ | $\begin{array}{r} .12 \\ .24 \\ .41 \\ .61 \\ \hline \end{array}$ | $\begin{array}{r} .13 \\ .24 \\ .44 \\ .67 \\ \hline \end{array}$ | $\begin{aligned} & .076 \\ & .13 \\ & .22 \\ & .35 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0095 \\ & .017 \\ & .033 \\ & \hline \end{aligned}$ | $\begin{aligned} & .044 \\ & .072 \\ & .12 \\ & .10 \\ & \hline \end{aligned}$ | $\begin{aligned} & .088 \\ & .15 \\ & .28 \\ & .41 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.1 \\ & 1.4 \\ & 2.0 \\ & 3.4 \\ & \hline \end{aligned}$ |
| 5.1 |  |  | .0048 .0058 .0081 .0095 | $\begin{array}{r} .018 \\ .021 \\ .022 \\ .033 \\ \hline \end{array}$ | $\begin{array}{r} .035 \\ .042 \\ .043 \\ .064 \\ \hline \end{array}$ | $\begin{array}{r} .005 \\ .042 \\ .042 \\ .003 \\ \hline \end{array}$ | $\begin{array}{r} .052 \\ .082 \\ .083 \\ .094 \\ \hline \end{array}$ | .035 .042 .043 .085 | $\begin{aligned} & .044 \\ & .052 \\ & .054 \\ & .080 \\ & \hline \end{aligned}$ | $\begin{array}{r} .014 \\ .053 \\ .055 \\ .013 \\ \hline \end{array}$ | .070 <br> .084 <br> .086 <br> .13 | $\begin{array}{r} .070 \\ .083 \\ .084 \\ .13 \\ \hline \end{array}$ | .0046 <br> .0056 <br> .0081 <br> .0095 | $\begin{array}{r} .044 \\ .052 \\ .053 \\ .079 \\ \hline \end{array}$ | $\begin{array}{r} .10 \\ .12 \\ .13 \\ \hline 19 \\ \hline \end{array}$ | $\begin{aligned} & 1.8 \\ & 2.3 \\ & 2.3 \\ & 3.3 \\ & \hline \end{aligned}$ |
| 5.1 |  | ( 40 Pn Diry <br> $(04 \mathrm{Pn}$ PGA) <br> ( 128 Min $P(A)$ | $\begin{aligned} & .028 \\ & .052 \\ & .11 \\ & \hline \end{aligned}$ | $\begin{array}{r} .061 \\ .11 \\ .23 \\ \hline \end{array}$ | $\begin{aligned} & .098 \\ & .18 \\ & .36 \\ & \hline \end{aligned}$ | $\begin{aligned} & .091 \\ & .16 \\ & .39 \\ & \hline \end{aligned}$ | $\begin{array}{r} .13 \\ .23 \\ .47 \\ \hline \end{array}$ | $\begin{array}{r} 12 \\ .21 \\ .44 \\ \hline \end{array}$ | $\begin{array}{r} .13 \\ .24 \\ .49 \\ \hline \end{array}$ | $\begin{aligned} & .17 \\ & .32 \\ & .65 \\ & \hline \end{aligned}$ | $\begin{array}{r} .22 \\ .39 \\ .11 \\ \hline \end{array}$ | $\begin{array}{r} .18 \\ .31 \\ .65 \\ \hline \end{array}$ | $\begin{aligned} & .028 \\ & .052 \\ & .11 \\ & \hline \end{aligned}$ | $\begin{array}{r} 11 \\ .20 \\ .42 \\ \hline \end{array}$ | $\begin{array}{r} .24 \\ .41 \\ .88 \\ \hline \end{array}$ | $\begin{array}{r} 3.3 \\ 5.6 \\ 12 \\ \hline \end{array}$ |
| 5.1 |  | $(40$ Pin DIV $(84$ Pin Poid <br> (12a Mn REA) | $\begin{aligned} & .048 \\ & .093 \\ & .19 \\ & \hline \end{aligned}$ | $\begin{aligned} & .089 \\ & .17 \\ & .34 \\ & \hline \end{aligned}$ | $\begin{array}{r} .13 \\ .24 \\ .49 \\ \hline \end{array}$ | $\begin{array}{r} 12 \\ .22 \\ .45 \\ \hline \end{array}$ | $\begin{array}{r} 16 \\ .29 \\ .60 \\ \hline \end{array}$ | $\begin{array}{r} .16 \\ .30 \\ .61 \\ \hline \end{array}$ | $\begin{array}{r} .17 \\ .32 \\ .86 \\ \hline \end{array}$ | $\begin{aligned} & .24 \\ & .45 \\ & .90 \\ & \hline \end{aligned}$ | $\begin{array}{r} .28 \\ .52 \\ 1.1 \\ \hline \end{array}$ | $\begin{array}{r} .22 \\ .40 \\ .82 \\ \hline \end{array}$ | $\begin{aligned} & .048 \\ & .093 \\ & .19 \\ & \hline \end{aligned}$ | $\begin{array}{r} 15 \\ .27 \\ .54 \\ \hline \end{array}$ | $\begin{array}{r} .28 \\ .50 \\ 1.0 \\ \hline \end{array}$ | $\begin{array}{r} 3.4 \\ 5.6 \\ 12 \\ \hline \end{array}$ |

MIL-HDBK-217F
NOTICE 1
APPENDIX A: PARTS COUNT

| Sisetion | Patlypo | $\begin{aligned} & \text { Environ. } \\ & T_{J}(\circ C) \rightarrow \end{aligned}$ | $\begin{aligned} & \mathrm{G}_{8} \\ & 50 \end{aligned}$ | $\begin{aligned} & G_{F} \\ & 60 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{G}_{\mathrm{M}} \\ & 65 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{N}_{5} \\ & 60 \end{aligned}$ | $\begin{aligned} & \hline N_{u} \\ & 65 \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{1 K} \\ & 75 \end{aligned}$ | $\begin{aligned} & \hline \mathbf{A}_{\mathbf{F}} \\ & 75 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { AUC } \\ & 90 \end{aligned}$ | $\begin{gathered} A_{U F} \\ 90 \end{gathered}$ | $\begin{gathered} A_{R W} \\ 75 \end{gathered}$ | $\begin{aligned} & \hline \mathrm{S}_{\mathrm{f}} \\ & 50 \\ & \hline \end{aligned}$ | $\begin{aligned} & M_{F} \\ & 65 \end{aligned}$ | $\begin{aligned} & \hline M_{L} \\ & 75 \end{aligned}$ | $C_{L}$ 60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.2 |  |  | $\begin{array}{r} .0047 \\ .0059 \\ .0067 \\ \hline \end{array}$ | $\begin{array}{r} .018 \\ .022 \\ .023 \\ .038 \end{array}$ | $\begin{array}{r} .038 \\ .043 \\ .045 \\ .088 \end{array}$ | $\begin{aligned} & .035 \\ & .042 \\ & .044 \\ & .068 \end{aligned}$ | $\begin{aligned} & .053 \\ & .063 \\ & .068 \\ & .098 \end{aligned}$ | $\begin{aligned} & .037 \\ & .045 \\ & .048 \\ & .075 \end{aligned}$ | .045 .055 .059 .090 | $\begin{aligned} & .80 \\ & .0 .18 \\ & .0180 \\ & .088 \\ & .11 \end{aligned}$ | $\begin{aligned} & .90 \\ & .074 \\ & .090 \\ & .099 \\ & .15 \end{aligned}$ | $\begin{aligned} & 10 \\ & \\ & .071 \\ & .086 \\ & .089 \\ & .14 \end{aligned}$ | .0047 .0059 .0067 .011 |  | $\begin{aligned} & 13 \\ & \hline .11 \\ & .13 \\ & .13 \\ & .20 \end{aligned}$ | $\begin{aligned} & 1.9 \\ & 2.3 \\ & 2.3 \\ & 3.3 \end{aligned}$ |
| 5.2 | Momorios PATOM, UVEPPRSM, EEPROM, EAPROM EEADG: Up io iok 18K 10 64M 64K 10 2501K 256K $\quad 1 \mathrm{MB}$ | $\begin{aligned} & \text { (24 Pin DFF } \\ & \text { (2A Pin DFF' } \\ & \text { (28 Pn DFF' } \\ & (40 \text { Pn DFF' } \end{aligned}$ | $\begin{array}{r} .0049 \\ .0061 \\ .0072 \\ .012 \\ \hline \end{array}$ | $\begin{array}{r} .018 \\ .022 \\ .024 \\ .038 \\ \hline \end{array}$ | $\begin{aligned} & .036 \\ & .044 \\ & .046 \\ & .077 \\ & \hline \end{aligned}$ | $\begin{array}{r} .036 \\ .043 \\ .045 \\ .068 \\ \hline \end{array}$ | $\begin{aligned} & .053 \\ & .084 \\ & .087 \\ & .10 \\ & \hline \end{aligned}$ | $\begin{aligned} & .037 \\ & .048 \\ & .051 \\ & .080 \\ & \hline \end{aligned}$ | $\begin{array}{r} .046 \\ .058 \\ .061 \\ .095 \\ \hline \end{array}$ | $\begin{aligned} & .049 \\ & .082 \\ & .073 \\ & .12 \\ & \hline \end{aligned}$ | $\begin{aligned} & .075 \\ & .093 \\ & .10 \\ & .16 \\ & \hline \end{aligned}$ | $\begin{array}{r} .072 \\ .087 \\ .092 \\ \hline 14 \\ \hline \end{array}$ | $\begin{aligned} & .0048 \\ & .0082 \\ & .0072 \\ & .012 \\ & \hline \end{aligned}$ | $\begin{aligned} & .045 \\ & .054 \\ & .057 \\ & .088 \end{aligned}$ | $\begin{array}{r} .11 \\ .13 \\ .13 \\ .20 \\ \hline \end{array}$ | $\begin{aligned} & 1.9 \\ & 2.3 \\ & 2.3 \\ & 3.3 \\ & \hline \end{aligned}$ |
| 5.2 |  | $\begin{aligned} & \text { (18 Pin DFFy } \\ & \text { (22 Pin OFF' } \\ & 124 \text { Pn DFF' } \\ & 128 \text { Pn DFFI } \end{aligned}$ | $\begin{array}{r} .0040 \\ .0055 \\ .0074 \\ .011 \\ \hline \end{array}$ | $\begin{array}{r} .014 \\ .019 \\ .023 \\ .032 \\ \hline \end{array}$ | $\begin{aligned} & .027 \\ & .036 \\ & .043 \\ & .057 \\ & \hline \end{aligned}$ | $\begin{array}{r} .027 \\ .034 \\ .040 \\ .053 \\ \hline \end{array}$ | $\begin{array}{r} .040 \\ .051 \\ .000 \\ .077 \\ \hline \end{array}$ | $\begin{aligned} & .029 \\ & .039 \\ & .049 \\ & .070 \\ & \hline \end{aligned}$ | $\begin{array}{r} .035 \\ .047 \\ .058 \\ .080 \end{array}$ | $\begin{aligned} & .040 \\ & .046 \\ & .078 \\ & .12 \end{aligned}$ | $\begin{aligned} & .059 \\ & .079 \\ & .10 \\ & .15 \\ & \hline \end{aligned}$ | $\begin{aligned} & .055 \\ & .070 \\ & .084 \\ & .11 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0040 \\ & .0055 \\ & .0074 \\ & .011 \\ & \hline \end{aligned}$ | $\begin{array}{r} .034 \\ .043 \\ .051 \\ .067 \\ \hline \end{array}$ | $\begin{aligned} & .080 \\ & .10 \\ & .12 \\ & .15 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.4 \\ & 1.7 \\ & 1.9 \\ & 2.3 \end{aligned}$ |
| 5.2 |  |  | $\begin{aligned} & .0079 \\ & .014 \\ & .023 \\ & .043 \\ & \hline \end{aligned}$ | $\begin{array}{r} .022 \\ .034 \\ .053 \\ .092 \\ \hline \end{array}$ | $\begin{aligned} & .038 \\ & .057 \\ & .084 \\ & .14 \\ & \hline \end{aligned}$ | $\begin{array}{r} .034 \\ .050 \\ .071 \\ .11 \\ \hline \end{array}$ | $\begin{aligned} & .050 \\ & .073 \\ & .10 \\ & .18 \\ & \hline \end{aligned}$ | $\begin{aligned} & .048 \\ & .077 \\ & .12 \\ & .22 \\ & \hline \end{aligned}$ | $\begin{array}{r} .054 \\ .085 \\ .13 \\ .23 \\ \hline \end{array}$ | $\begin{array}{r} .083 \\ .14 \\ .25 \\ .48 \\ \hline \end{array}$ | $\begin{array}{r} .10 \\ .17 \\ .27 \\ .49 \\ \hline \end{array}$ | $\begin{aligned} & .073 \\ & .11 \\ & .16 \\ & .26 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0079 \\ & .014 \\ & .023 \\ & .043 \\ & \hline \end{aligned}$ | $\begin{aligned} & .044 \\ & .065 \\ & .092 \\ & .15 \\ & \hline \end{aligned}$ | $\begin{aligned} & .098 \\ & .14 \\ & .19 \\ & .30 \\ & \hline \end{aligned}$ | $\begin{array}{r} 1.4 \\ 1.8 \\ 1.9 \\ .3 .3 \\ \hline \end{array}$ |
| 5.2 |  |  | $\begin{array}{r} .010 \\ .017 \\ .028 \\ .053 \\ \hline \end{array}$ | $\begin{aligned} & .0218 \\ & .043 \\ & .065 \\ & .12 \\ & \hline \end{aligned}$ | $\begin{aligned} & .050 \\ & .071 \\ & .10 \\ & .18 \\ & \hline \end{aligned}$ | $\begin{aligned} & .048 \\ & .0013 \\ & .065 \\ & .15 \end{aligned}$ | $\begin{aligned} & .087 \\ & .091 \\ & .12 \\ & .21 \\ & \hline \end{aligned}$ | $\begin{aligned} & .082 \\ & .095 \\ & .15 \\ & .27 \\ & \hline \end{aligned}$ | $\begin{aligned} & .070 \\ & .11 \\ & .18 \\ & .29 \\ & \hline \end{aligned}$ | $\begin{array}{r} .10 \\ .18 \\ .30 \\ .58 \\ \hline \end{array}$ | $\begin{array}{r} .13 \\ .21 \\ .33 \\ .81 \\ \hline \end{array}$ | $\begin{aligned} & .098 \\ & .14 \\ & .19 \\ & .33 \\ & \hline \end{aligned}$ | $\begin{aligned} & .010 \\ & .017 \\ & .028 \\ & .053 \\ & \hline \end{aligned}$ | $\begin{aligned} & .058 \\ & .081 \\ & .11 \\ & .19 \\ & \hline \end{aligned}$ | $\begin{array}{r} .13 \\ .18 \\ .23 \\ .39 \\ \hline \end{array}$ | $\begin{array}{r} 1.9 \\ 2.3 \\ 2.3 \\ 3.4 \\ \hline \end{array}$ |
| 5.2 |  |  | $\begin{aligned} & .0075 \\ & .012 \\ & .18 \\ & .033 \\ & \hline \end{aligned}$ | $\begin{array}{r} .023 \\ .033 \\ .045 \\ .079 \\ \hline \end{array}$ | $\begin{aligned} & .043 \\ & .058 \\ & .074 \\ & .13 \\ & \hline \end{aligned}$ | $\begin{aligned} & .041 \\ & .054 \\ & .065 \\ & .11 \\ & \hline \end{aligned}$ | $\begin{array}{r} .060 \\ .079 \\ .095 \\ .16 \\ \hline \end{array}$ | $\begin{aligned} & .050 \\ & .072 \\ & .10 \\ & .18 \\ & \hline \end{aligned}$ | $\begin{aligned} & .058 \\ & .083 \\ & .11 \\ & .20 \\ & \hline \end{aligned}$ | $\begin{aligned} & .077 \\ & .12 \\ & .19 \\ & .35 \\ & \hline \end{aligned}$ | $\begin{array}{r} .10 \\ .15 \\ .22 \\ 30 \\ \hline \end{array}$ | $\begin{aligned} & .084 \\ & .11 \\ & .14 \\ & .24 \\ & \hline \end{aligned}$ | $\begin{aligned} & .0075 \\ & .012 \\ & .18 \\ & .033 \\ & \hline \end{aligned}$ | $\begin{array}{r} .052 \\ .089 \\ .084 \\ .14 \\ \hline \end{array}$ | $\begin{array}{r} .12 \\ .15 \\ .18 \\ .30 \\ \hline \end{array}$ | 1.8 <br> 2.3 <br> 2.3 <br> 3.4 |
| 5.3 | VHSIC Norocialy CNOS |  |  | der 10 | cioon | VHSIC | MOS |  |  |  |  |  |  |  |  |  |
| 5.4 | GeAs NNMC (EII = 1.5 ) <br> 1 to 100 Eloments <br> 101 10 1000 Actipe Elomens <br>  | (8 Pn DPP) (16 Pin DW ${ }^{1}$ ) | $\begin{aligned} & .0013 \\ & .0028 \end{aligned}$ | $\begin{aligned} & .0052 \\ & .011 \end{aligned}$ | $\begin{aligned} & .010 \\ & .022 \end{aligned}$ | $\begin{aligned} & .010 \\ & 0202 \end{aligned}$ | $\begin{aligned} & .018 \\ & .034 \end{aligned}$ | $\begin{aligned} & .011 \\ & .023 \end{aligned}$ | $\begin{aligned} & .013 \\ & .028 \end{aligned}$ | $\begin{aligned} & .015 \\ & .030 \end{aligned}$ | $\begin{aligned} & .022 \\ & .047 \end{aligned}$ | $.021$ | $\begin{aligned} & .0013 \\ & .0028 \end{aligned}$ | $\begin{aligned} & .013 \\ & .028 \end{aligned}$ | $\begin{aligned} & .031 \\ & .068 \end{aligned}$ | ${ }_{1.2}^{.57}$ |
| 5.4 | $\begin{aligned} & \text { Geas Digh (Ee }=1.4) \\ & 101000 \text { Active Elomensa } \\ & 1001 \text { io } 10,000 \text { Active Elements } \end{aligned}$ | $\begin{aligned} & (38 \mathrm{Pin} \mathrm{DIP}) \\ & (64 \text { Pin PGA) } \end{aligned}$ | $\begin{aligned} & .0086 \\ & .013 \\ & \hline \end{aligned}$ | $\begin{array}{r} .028 \\ .050 \\ \hline \end{array}$ | $\begin{array}{r} .052 \\ .10 \\ \hline \end{array}$ | $.052$ | $\begin{aligned} & .078 \\ & 15 \end{aligned}$ | $\begin{aligned} & .054 \\ & .10 \end{aligned}$ | $\begin{aligned} & .087 \\ & 13 \end{aligned}$ | $.078$ | $\begin{array}{r} 12 \\ .23 \end{array}$ | $\begin{array}{r} 11 \\ .20 \\ \hline \end{array}$ | $\begin{aligned} & .0066 \\ & .013 \\ & \hline \end{aligned}$ | $\begin{array}{r} .065 \\ .13 \\ \hline \end{array}$ | $\begin{array}{r} .16 \\ .30 \end{array}$ | 2.9 <br> 5.5 |



APPENDIX A: PARTS COUNT


NOTICE 1
APPENDIX A: PARTS COUNT
Cimentic Fallure Rave - $\lambda_{0}$ (Fillures $/ 10^{6}$ Howrs) for Dlecrete Semiconductors (cont'd)

| Seration | Pant Type | $\begin{aligned} & \text { Env. } \rightarrow a_{B} \\ & T_{y}(C) \rightarrow 50 \end{aligned}$ | $\begin{aligned} & a_{F} \\ & \infty \end{aligned}$ | $\begin{aligned} & a_{M} \\ & 65 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{N}_{\mathrm{S}} \\ & 60 \end{aligned}$ | $\begin{aligned} & N_{v} \\ & \infty \end{aligned}$ | $\begin{aligned} & A_{1} \\ & 75 \end{aligned}$ | $\begin{aligned} & A_{1 F} \\ & 75 \end{aligned}$ | $\begin{aligned} & A_{u c} \\ & 90 \end{aligned}$ | $\begin{aligned} & A_{U F} \\ & 90 \end{aligned}$ | $\begin{gathered} A_{\mathrm{PN}} \\ 75 \end{gathered}$ | $\begin{aligned} & s_{F} \\ & 50 \end{aligned}$ | $\begin{aligned} & M_{F} \\ & 65 \end{aligned}$ | $\begin{aligned} & M_{L} \\ & 75 \end{aligned}$ | $\begin{aligned} & c_{1} \\ & \text { so } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | opto-mectrionics |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6.11 | Photodetector | . 011 | . 029 | . 13 | . 074 | . 20 | . 084 | 13 | 17 | 23 | 36 | 0057 | 15 | . 51 | 6.6 |
| 6.11 | Optoteocrear | . 027 | . 070 | . 31 | . 17 | . 47 | . 20 | . 30 | 42 | . 56 | 85 | . 013 | . 35 | 1.2 | 16 |
| 6.11 | Empres | . 00047 | . 0012 | . 0056 | . 0031 | . 0084 | . 0035 | . 0053 | . 0074 | 0098 | 015 | . 00324 | . 0067 | . 021 | 28 |
| 6.12 | Aphaxumerce Dimplay | . 0062 | . 016 | 073 | 040 | . 11 | . 046 | . 069 | . 096 | . 13 | 20 | . 0031 | 082 | 28 | 3.6 |
| 0.13 | Lreor Dloco. CraneN Gans | 5.1 | 16 | 78 | 39 | 120 | 58 | 86 | ${ }^{\infty}$ | 110 | 240 | 2.6 | 87 | 350 | 3500 |
| 6.13 |  | 9.0 | 28 | 135 | 69 | 200 | 100 | 150 | 150 | 200 | 403) | 4.5 | 150 | 600 | 6200 |
| 7 | tuass | 5 | Seation | Hnctuca | Focative | CRTE, | Fror | Inptiore | ystrone | WTs, M | errons) |  |  |  |  |
| 8 | Lasers |  | seator | 。 |  |  |  |  |  |  |  |  |  |  |  |




| $\begin{gathered} \text { Section } \\ \hline \end{gathered}$ | Pert Type or Diencetric | Sirle | Minc- | $\begin{aligned} & E_{N v} \rightarrow G_{B} \\ & T_{A}(C) \rightarrow 30 \end{aligned}$ | ${ }_{4}^{C_{F}}$ | $G_{4}$ | $\begin{aligned} & \mathrm{N}_{\mathrm{s}} \\ & 40 \end{aligned}$ | $\begin{aligned} & h_{U} \\ & 45 \end{aligned}$ | $\begin{aligned} & A_{1 C} \\ & 55 \end{aligned}$ | $\begin{aligned} & \hline A_{I F} \\ & 55 \end{aligned}$ | $\begin{aligned} & 4_{14} \\ & 70 \end{aligned}$ | $\begin{aligned} & \lambda_{u F} \\ & 70 \end{aligned}$ | $\begin{aligned} & A_{\text {RW }} \\ & 55 \end{aligned}$ | $\begin{aligned} & \mathcal{S}_{\mathrm{F}} \\ & 30 \end{aligned}$ | $\begin{aligned} & M_{F} \\ & 45 \end{aligned}$ | $\begin{gathered} M_{L} \\ 55 \end{gathered}$ | $C_{1}$ 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10.1 | Paper. By Pase | ${ }_{\sim}$ | 25 | . 0038 | . 0072 | . 033 | 018 | . 055 | . 023 | 03 | 070 | . 13 | . 083 | . 0018 | . 044 | . 12 | 2.1 |
| 10.1 | Paper, ByPases | CA | 12800 | . 0039 | . 0087 | . 042 | 022 | . 070 | . 035 | . 047 | . 19 | . 35 | . 13 | . 002 | . 056 | . 19 | 2.5 |
| 10.2 | Pepempliaric. Foeat orrough | GRT | 11003 | . 0047 | . 0096 | . 044 | . 034 | . 073 | . 030 | . 040 | . 094 | . 15 | . 11 | . 0024 | . 058 | . 16 | 2.7 |
| 10.3 | Preariflatic Fimm | CPV | 14157 | 0021 | . 0042 | . 017 | . 010 | . 030 | . 0088 | 013 | . 026 | . 048 | . 044 | . 0010 | . 023 | . 063 | 1.1 |
| 10.3 | Puperfitaste Fim | COR | 19979 | . 0021 | . 0042 | . 017 | . 010 | . 030 | 0088 | . 013 | . 026 | . 048 | . 044 | . 0010 | . 023 | . 063 | 1.1 |
| 10.4 | Moselitred Paperplastic | वR | 30022 | . 0029 | . 0058 | . 023 | . 014 | . 041 | . 012 | 018 | . 037 | . 066 | . 060 | . 0014 | . 032 | 088 | 1.5 |
| 10.4 | Monilized Pinita Plastic | CH | 18912 | . 0029 | . 0058 | . 023 | 014 | . 041 | . 012 | 018 | . 037 | . 066 | 060 | . 0014 | . 032 | . 088 | 1.5 |
| 10.5 | Mcmilied PaperPieate | CFR | 55514 | . 0041 | . 0083 | . 042 | . 021 | . 067 | . 026 | . 048 | 086 | 14 | . 10 | . 0020 | . 054 | . 15 | 2.5 |
| 10.8 | Mcmelized Plasuc | CPH | 83421 | . 0023 | . 0092 | . 019 | 012 | . 033 | . 0096 | . 014 | . 034 | . 053 | . 048 | . 0011 | . 026 | . 07 | 1.2 |
| 10.7 | MICA (Dpped er Moideal | CWA | 39001 | . 0005 | . 0015 | . 0091 | . 0044 | . 014 | . 0068 | . 0095 | . 054 | . 069 | 031 | . 00025 | . 012 | . 046 | 45 |
| 10.7 | mica (0ppedt | Cn | 5 | . 0005 | . 0015 | . 0091 | . 0044 | . 014 | . 0068 | . 0095 | . 054 | . 060 | 031 | . 00025 | . 012 | . 046 | . 45 |
| 10.8 | MICA fevions | CB | 10050 | . 018 | . 037 | . 19 | . 094 | . 31 | . 10 | . 14 | 47 | . 60 | . 48 | . 0091 | . 25 | . 68 | 11 |
| 10.9 | Glase | CrA | 23280 | . 00032 | . 00098 | . 0059 | . 0029 | . 0094 | . 0044 | . 0062 | . 035 | . 046 | . 020 | . 00016 | . 0078 | . 030 | . 29 |
| 10.9 | Glase | cr | 11272 | .00032 | . 00088 | . 0050 | . 0029 | . 0094 | . 0044 | . 0062 | . 035 | . 046 | 020 | . 00016 | . 0076 | . 030 | 29 |
| 10.10 | Cerunte (Gen Pupoer) | $\mathrm{CK}^{\prime}$ | 11915 | . 0036 | . 0074 | . 034 | . 019 | . 056 | . 015 | . 015 | . 092 | . 048 | . 077 | . 0014 | . 049 | . 13 | 2.3 |
| 10.10 | Carante (Gion Pupowe) | CNA | 39014 | . 0038 | . 0074 | . 034 | . 019 | . 058 | . 015 | . 015 | . 032 | . 048 | 077 | . 0014 | . 049 | . 13 | 2.3 |
| 10.11 | Cersuric (Tompa Cormp) | $\sim_{C}$ | 20 | .00078 | . 0022 | . 013 | . 0056 | . 023 | . 0077 | . 015 | . 053 | . 12 | 046 | . 00039 | . 017 | . 085 | 68 |
| 10.11 | Censote Chip | Con | 55881 | .00078 | . 0022 | . 013 | . 0056 | . 023 | . 0077 | . 015 | . 053 | . 12 | . 046 | . 00039 | . 017 | . 065 | . 68 |
| 10.12 | Triniom, 8014 | Csp | 38000 | . 0018 | . 0039 | . 016 | . 0097 | . 028 | . 0091 | . 011 | . 034 | . 057 | 055 | . 00072 | . 022 | . 066 | 1.0 |
| 10.13 | Tramem, Morrsold | as | 38008 | . 0081 | . 013 | . 069 | . 039 | . 11 | . 031 | .061 | . 13 | 29 | . 18 | . 0030 | . 089 | 26 | 4.0 |
| 10.13 | Tormam, Mor-Sold | $a$ | 3885 | . 0081 | . 013 | . 069 | . 038 | . 11 | . 031 | . 061 | . 13 | 29 | . 18 | . 0030 | . 089 | 28 | 4.0 |
| 10.14 | Auminum Oade | an | 39018 | . 024 | . 081 | . 42 | . 18 | . 59 | 46 | 55 | 2.1 | 2.6 | 1.2 | . 012 | . 49 | 1.7 | 21 |
| 10.15 | Aknirum Dy | CE | 62 | . 020 | . 081 | . 58 | 24 | . 83 | . 73 | 88 | 4.3 | 5.4 | 2.0 | . 015 | . 68 | 2.8 | 28 |
| 10.16 | Verieto, Corrartic | cV | 81 | . 00 | . 27 | 1.2 | . 71 | 2.3 | . 69 | 1.1 | 6.2 | 12 | 4.1 | . 032 | 1.9 | 5.9 | 85 |
| 10.17 | Verietio, Fiven | PC | 14000 | . 033 | . 13 | . 62 | . 31 | . 93 | . 21 | 28 | 2.2 | 3.3 | 2.2 | . 016 | . 93 | 3.2 | 37 |
| 10.18 | Varnela, Ar Timmer | CT | 92 | . 000 | . 33 | 1.6 | . 87 | 3.0 | 1.0 | 1.7 | 9.9 | 10 | 6.1 | . 040 | 2.5 | 8.9 | 100 |
| 10.19 | Verable Veamm | 0 | 23180 | 0.4 | 1.3 | 6.7 | 3.6 | 13 | 5.7 | 10 | 58 | 90 | 23 | . 20 | . | . |  |
| NOTE: $1{ }^{-}$- Not Morrally ueed in tha Ef <br> a $T_{A}=$ Dotmill Compormen Antion |  |  |  | ontrorment vent Tormperalur | $\text { ( }{ }^{(C)}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Quatly |  | S Established Renability Syles |  |  |  | Mnl-SPEC |  | $\frac{\text { Lover }}{10}$ |  |  |  |  |  |

MIL-HDBK-217F
NOTICE 1
APPENDIX A: PARTS COUNT


[^0]Coneric Fallure Rete, $\lambda_{\mathrm{g}}$ (Fallures/10 $0^{6}$ Hours) for Miscellencous Parts

| $\begin{gathered} \text { Section } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Por Type } \\ & \text { Devectic } \end{aligned}$ | MR. | $\begin{aligned} & E m_{v} \rightarrow \sigma_{B} \\ & T_{A}(c) \rightarrow 30 \end{aligned}$ | $\begin{aligned} & G_{F} \\ & 40 \end{aligned}$ | $\begin{aligned} & G_{M} \\ & 45 \end{aligned}$ | $\begin{gathered} \mathrm{N}_{\mathrm{S}} \\ 40 \end{gathered}$ | $\begin{aligned} & N_{U} \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{1 C} \\ & 55 \end{aligned}$ | $\begin{aligned} & A_{\text {IF }} \\ & 55 \\ & \hline \end{aligned}$ | $\begin{aligned} & A_{U C} \\ & 70 \end{aligned}$ | $\begin{aligned} & A_{1 F} \\ & 70 \end{aligned}$ | $\begin{gathered} A_{\text {PW }} \\ 55 \end{gathered}$ | $\begin{aligned} & \mathrm{S}_{\mathrm{F}} \\ & 30 \end{aligned}$ | $\begin{aligned} & M_{F} \\ & 45 \end{aligned}$ | $\begin{aligned} & M_{l} \\ & 55 \end{aligned}$ | $\begin{aligned} & G_{2} \\ & 40 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SNGLE CONECTIONS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 17.1 | Hend Sotter, wo Wrapping |  | . 0028 | . 0052 | 018 | . 010 | . 029 | . 010 | . 016 | . 016 | . 021 | . 042 | . 0013 | . 023 | . 062 | 1.1 |
| 17.1 | Hend Sodier, wWreppha |  | . 00014 | . 00028 | . 00098 | . 00056 | . 0015 | . 00056 | . 00084 | . 00004 | . 0011 | . 0022 | . 00007 | . 0013 | . 0034 | 059 |
| 17.1 | Comp |  | . 00028 | . 00052 | . 0018 | . 0010 | . 0020 | . 0010 | . 0016 | . 0016 | . 0021 | . 0042 | . 00013 | . 0023 | . 0062 | . 11 |
| 17.1 | Wed |  | . 000050 | . 000100 | . 000350 | . 000200 | . 000550 | . 000200 | . 000300 | . 000300 | . 000400 | . 000800 | . 000025 | . 000450 | . 001200 | . 021000 |
| 17.1 | Sotberieno Whep |  | . 0000035 | . 000007 | . 000025 | . 000014 | . 000039 | . 000014 | . 000021 | . 000021 | .000028 | . 000056 | . 0000018 | . 000031 | . 000084 | 0015 |
| 17.1 | Clip Tammation |  | . 00012 | . 00024 | 00084 | . 00048 | . 0013 | .00048 | . 00072 | . 00072 | . 00096 | . 0019 | . 00006 | . 0011 | . 0029 | . 050 |
| 17.1 | Achow Solde |  | . 000068 | . 000138 | . 000483 | . 000278 | . 000759 | . 000278 | . 000414 | . 000214 | . 000552 | . 001104 | . 000035 | . 000621 | . 001656 | 02898 |
|  | METERS, PXNEL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18.1 | OC Anmaterar ortomer | M-1030 | 0.09 | 0.36 | 2.3 | 1.1 | 3.2 | 2.5 | 3.8 | 5.2 | 8.6 | 5.4 | 0.099 | 5.4 | N/A | N/A |
| 18.1 | AC Amonerer or Vothater | M-1050n | 0.15 | 0.61 | 3.8 | 1.8 | 5.4 | 4.3 | 6.4 | 8.0 | 11 | 9.2 | 0.17 | 8.2 | N/A | N/A |
| 19.1 | Ount Cryan | C-3008 | . 032 | . 096 | . 32 | . 18 | . 51 | . 38 | . 54 | . 70 | . 90 | 14 | . 016 | .42 | 1.0 | 16 |
| 20.1 | Lempe, moendecoerst, AC |  | 3.9 | 7.8 | 12 | 12 | 16 | 16 | 16 | 19 | 23 | 19 | 2.7 | 16 | 23 | 100 |
| 20.1 | Lempe, haendencent, DC |  | 13 | 26 | 38 | 38 | 51 | 51 | 51 | 64 | 77 | 64 | 0.0 | 51 | 77 | 350 |
|  | ELECTRONC FLITERS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21.1 | Cementofarito | F.15738 | . 022 | . 044 | . 13 | . 088 | . 20 | . 15 | . 20 | . 24 | . 29 | 24 | . 018 | . 15 | . 33 | 2.8 |
| 21.1 | Divarum LC Comp | F-15733 | . 12 | 24 | . 72 | . 48 | 1.1 | . 84 | 1.1 | 1.3 | 1.6 | 1.3 | . 096 | . 84 | 4.8 | 14 |
| 21.1 |  | F-18027 | . 27 | 54 | 1.6 | 1.1 | 2.4 | 1.9 | 2.4 | 3.0 | 9.5 | 3.0 | . 22 | 1.9 | 4.1 | 32 |
| 22.1 | Fuses |  | . 010 | . 020 | . 080 | . 050 | . 11 | . 090 | . 12 | . 15 | . 18 | 16 | . 009 | . 10 | 21 | 2.3 |

## MIL-HDBK-217F

$\pi_{\mathrm{Q}}$ Factor for Use with Section $\mathbf{1 1 - 2 2}$ Devices

| Section \# | Pant Type | $\begin{gathered} \hline \text { Established } \\ \text { Reliability } \end{gathered}$ | MIL-SPEC | Non-MIL |
| :---: | :---: | :---: | :---: | :---: |
| 11.1, 11.2 | Inductive Devices | .25* | 1.0 | 10 |
| 12.1, 12.2, 12.3 | Rotating Devices | N/A | N/A | N/A |
| 13.1 | Retays, Merchanical | . 60 | 3.0 | 9.0 |
| 13.2 | Relays, Solid State and Time Delay (H)brid \& Solid State) | N/A | 1.0 | 4 |
| 14.1, 14.2 | Swilches, Toggle, Pushbutton, Sensitive | N/A | 1.0 | 20 |
| 14.3 | Switches, Rotary Water | N/A | 1.0 | 50 |
| 14.4 | Swhiches, Thuintwheel | N/A | 1.0 | 10 |
| 14.5 | Clrcult Breakers, Thermal | N/A | 1.0 | 8.4 |
| 15.1, 15.2, 15.3 | Connectors | N/A | 1.0 | 2.0 |
| 16.1 | Interconnection Assemblies | N/A | 1.0 | 2.0 |
| 17.1 | Connections | N/A | N/A | N/A |
| 18.1 | Meters, Panel | N/A | 1.0 | 3.4 |
| 19.1 | Quartz Crystals | N/A | 1.0 | 2.1 |
| 20.1 | Lamps, Incandescent | N/A | N/A | N/A |
| 21.4 | Electronic Fillers | N/A | 1.0 | 2.9 |
| 22.1 | Fuses | N/A | N/A | N/A |

[^1]APPENDIX A: PARTS COUNT

Default Parameters for Dlscrete Semlconductors


## MIL-HDBK-217F NOTICE 1

| Default Parametors for Fesistors |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Part Type | Sryte | MIL-R-SPEC | ${ }^{\prime}$ R | $\pi$ | ${ }^{\text {T TAPS }}$ | Cominents |
| 9.1 9.1 | Composition Compostion | ${ }_{\text {FICR }}$ | 39008 11 | $\begin{aligned} & 1.1 \\ & 1.1 \end{aligned}$ |  |  | Pw. Stess = 5, 1M ohm Pwr. Stress = 5. 1 Mohm |
| 9.2 | Film, Insulated | FLR | 39017 | 1.1 |  |  | Pwr. Stress = 5, 1 M ohm |
| 9.2 | Film, Insulated | RL | $2 ? 684$ | 1.1 |  |  | Pwr. Stress $=5.1 \mathrm{M} \mathrm{ohm}$ |
| 9.2 | Fim, RN(R,Cor $N$ ) | FNR | 55182 | 1.1 |  |  | Pwr. Stress $=5.1 \mathrm{~N}$ ohm |
| 9.2 | Fim | FN | 10509 | 1.1 |  |  | Pwr. Stress = 5, 1 N chm |
| 9.3 9.4 | Film. Povver Fixed, Notwork | $\begin{aligned} & \text { PD } \\ & \text { RZ } \end{aligned}$ | $\begin{aligned} & 11804 \\ & 83401 \end{aligned}$ | 1.0 |  |  | Pwr. Stress = 5, 100 ohm <br> Pur. Stress $=.5, T_{C}=T_{A}+28^{\circ} \mathrm{C}$, 10 Film Resistors |
| 9.5 | Wrewound, Accurate | FBR | 39005 | 1.7 |  |  | Pwr. Stress $=5,100 \mathrm{~K}$ ohms |
| 9.5 | Wrewound, Accisrate | RB | 93 | 1.7 |  |  | Pwr. Stress = 5, 100 K ohms |
| 9.6 | Wrowound, Power | FWR | 39007 | 1.1 |  |  | $P^{\text {PWr. Stress }}=.5,5 \mathrm{~K}$ ohms, RWR 84 |
| 9.6 | Wrewound, Power | RW | 26 | 1.0 |  |  | Pwr. Stress $=.5,5 \mathrm{~K}$ ohms. AW10 |
| 9.7 | Wirewound, Power, Charsts Mountad | PER | 39009 | 1.1 |  |  | Pwr. Stress = .5. Noninductlvely Wound, 5K ohm, RER 55 |
| 9.7 | Wrewound, Power, Chassts Mounterd | RE | 18546 | 1.1 |  |  | PWr. Stress $=.5, \mathrm{MIL}-\mathrm{R}-18546$, Char. N, 5K ohm, RE75 |
| 8.8 | Thermistor | HTH | 236413 |  |  |  | Disk Type |
| 9.9 | Wrowound, Verinble | PIR | 39015 | 1.4 | 1.1 | 1.0 | Pwr. Stress = 5, 5K ohms, 3 Taps, Voltage Stress $=.1$ |
| 9.9 9.10 | Wrowound, Vartable Wrewound, Variable, Procision | RT | 27208 12934 | 1.4 | 1.1 1.1 | 1.0 1.0 | PWr. Siress $=5,3$ Taps, Voltage Stresti $=.1$ Pur. Siress $=5$, Construction Class $5(\pi=1.5)$ |
| 9.10 9.11 | Wrewound, Veriabie, Procision | PR | 12934 19 | 1.4 1.4 | 1.1 1.0 | 1.0 1.0 | Pwr. Siress $=.5$, Construction Class $5\left(\pi_{c}=1.5\right)$. <br> 50K ohm, 3 Taps, Voltage Siress = . 1 <br> PWr. Siress $=5,5 \mathrm{~K}$ ohms, 3 Taps, Voltage Stress = 5 |
| 9.11 | Wirewound, Variable, Semipreciston | PA | 19 | 1.4 | 1.0 | 1.0 | Pwr. Siress = b, bk ohms, 3 Taps, Voitage Stress m. 5 |
| 9.11 | Wrimound, Senilpreciston | $\begin{aligned} & \text { PK } \\ & \text { OK } \end{aligned}$ | 39002 | $1.4$ | 1.0 1.0 | $1.0$ |  |
| 9.12 | Wirmound, Variable, Power | PP | 22 | 1.4 | 1.0 | 1.0 | Pwr. Stress $=5,3$ Taps, Voltage Stessis $=.5$, Unenclosed ( $\pi_{c}=1$ ) |
| 9.13 | Nonwirewound, Vartable | RNR | 39035 | 1.2 | 1.0 | 1.0 | Pwr. Stress $=5.5200 \mathrm{Kohm}, 3$ Taps, Voltage Stress $=.5$ |
| 9.13 | Nonwtrewound, Variable | RJ | 22097 | 1.2 | 1.0 | 1.0 | Pwr. Stress = .5, 200 K ohm, 3 Taps, Voltagi Stress $=.5$ |
| 9.14 | Comporition, Varlable | RN | 94 | 1.2 | 1.0 | 1.0 | Pwr. Stress $=5,270 \mathrm{~K}$ ohm, 3 Taps, Voltage Stoss $=.5$ |
| 9.15 | Nonwrewound, Variable Precision | RO | 39023 | 1.2 | 1.0 | 1.0 | Pwr. Stiesis $=.5,200 \mathrm{Kohm}$,3 Taps, Voltage Stress $=.5$ |
| 9.15 | Fim, Vartable | FVC: | 23285 | 1.2 | 1.0 | 1.0 | Pwr. Stess $=.5$ 200K ohm, 3 Taps, Voltage Stress $=.5$ |

Default Parameters for Capacitors

| Section | Part Type or | Style | MIL-C-SPEC | ${ }^{\pi} \mathrm{CV}$ | Temp. Rating | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10.1 | Paper, By-Pass | ${ }^{\text {c }}$ | 25 | 1.0 | 125 | Voltage Stress $=.5, .15 \mu \mathrm{~F}$ |
| 10.1 | Paper, By-Pass | CA | 12889 | 1.0 | 85 | Voltage Stress $=.5, .15 \mu \mathrm{~F}$ |
| 10.2 | Paper/Plastic, Feed-through | CZR | 11693 | 1.0 | 125 | Voltage Stress $=.5$, $.061 \mu \mathrm{~F}$ |
| 10.3 | Paper/Plastic Film | CPV | 14157 | 1.0 | 125 | Voltage Stress $=.5, .027 \mu \mathrm{~F}$ |
| 10.3 | Papor/Plastic Fllm | CAR | 19978 | 1.0 | 125 | Volage Stress $=.5$, $.033 \mu \mathrm{~F}$ |
| 10.4 | Metalized Paper/Plastic | CH | 39022 | 1.0 | 125 | Voltage Stress $=.5, .14 \mu \mathrm{~F}$ |
| 10.4 | Metallized Plastic/Plastic | CH | 18312 | 1.0 | 125 | Voltage Stress $=.5, .14 \mu \mathrm{~F}$ |
| 10.5 | Metalized PaperPlastic | CPR | 55514 | 1.0 | 125 | Voltage Stress $=.5 . .33 \mu \mathrm{~F}$ |
| 10.6 | Metallized Plastic | CPH | 83421 | 1.0 | 125 | Voltage Stress $=.5, .14 \mu \mathrm{~F}$ |
| 10.7 10.7 | MICA (Dipped or Molded) | CMR | 39001 | 1.0 | 125 | Voltage Stress $=.5,300 \mathrm{pF}$ |
| 10.8 | MICA (Dipped) MICA (Bution) | CM | 5 | 1.0 | 125 | Voltage Stress $=.5,300 \mathrm{pF}$ |
| 10.9 | Glass | CYR | 10950 23269 | 1.0 1.0 | 150 125 | Voltage Stress $=.5,160 \mathrm{pF}$ |
| 10.9 | Glass | Cr | 11272 | 1.0 | 125 | Voltage Stress = .5.30 pF |
| 10.10 | Ceramic (Gen. Purpose) | ck | 11015 | 1.0 | 125 | Voltage Stress $=.5,3300 \mathrm{pF}$ |
| 10.10 | Ceramic (Cen. Puppee) | CKR | 39014 | 1.0 | 125 | Voltage Stress $=.5,3300 \mathrm{pF}$ |
| 10.11 10.11 | Cerminic (Tomp. Comp.) | COR | 20 | 1.0 | 125 | Votage Stress $=.5 .81 \mathrm{pF}$ |
| 10.12 | leremic chip | COR | 55681 39003 | 1.0 1.0 | 125 125 | Voltage Stress $=$.5, 81 pF |
|  |  |  |  |  |  | resistance, $\pi_{S R}=.13$ |
| 10.13 | Tenmum, Non-Solld | CLR | 39006 | 1.0 | 125 | Voltage Stress $=.5$, Foil, Hermetic, $20 \mu \mathrm{~F}, \pi_{\mathrm{C}}=1$ |
| 10.13 | Tenmum, Non-Solld | a | 3965 | 1.0 | 125 | Voltage Stress $=.5$, Foil, Hermetic, $20 \mu \mathrm{~F}, \pi_{\mathrm{c}}=1$ |
| 10.14 | Auminum Oxide | CuR | 39018 | 1.3 | 125 | Voltage Stress $=.5 .1700 \mu \mathrm{~F}$ |
| 10.15 | Aluminum Dry | CE | 62 | 1.3 | 85 | Voltage Stress $=.5,1600 \mu \mathrm{~F}$ |
| 10.16 10.17 | Variable, Ceramic Variable, Piston | CV | 81 |  | 85 | Voltage Stress $=.5$ |
| 10.18 | Variabbe, Piston Varkble, Ak Trimmer | PC CT | 14409 92 |  | 125 | Voltage Stress $=.5$ |
| 10.19 | Variable, Vacuum | cG | 23183 |  | 85 | Voltage Stress $=.5$, Variable Configuration |

APPENDIX A: PARTS COUNT



[^0]:    

[^1]:    - Category applies onty to MIL-C-39010 Coils.

